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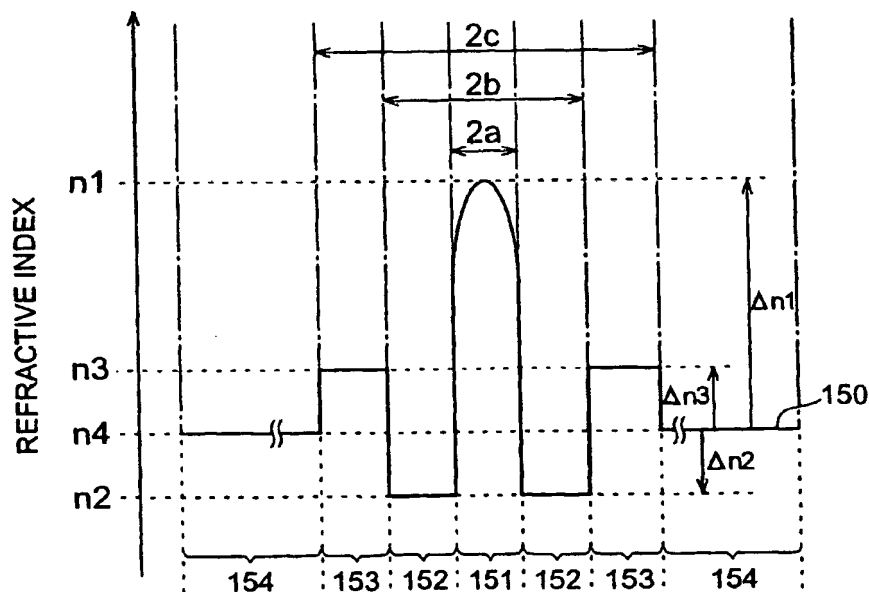
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(54) Title: **DISPERSION-COMPENSATING OPTICAL FIBER WITH W-SHAPED INDEX PROFILE**



(57) Abstract: The invention is directed to a dispersion-compensating optical fiber which can compensate for the chromatic dispersion and dispersion slope of a non-zero dispersion-shifted optical fiber by a short length. The dispersion-shifted optical fiber constitutes an optical transmission line together with a dispersion-compensating optical fiber fusion-spliced thereto. The dispersion-compensating optical fiber has, at a wavelength of 1550 nm, a chromatic dispersion D_{DCF} of -40 ps/nm/km or less and a ratio (D_{DCF}/S_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of 0.005/nm or more.

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DISPERSION-COMPENSATING OPTICAL FIBER WITH W-SHAPED INDEX PROFILE

DESCRIPTION

Dispersion-Compensating Optical Fiber, and, Optical
Transmission Line and Dispersion-Compensating Module
respectively including the Same

5 **Technical Field**

The present invention relates to a
dispersion-compensating optical fiber which compensates for
the chromatic dispersion and dispersion slope of a
dispersion-shifted optical fiber, an optical transmission
10 line including the dispersion-shifted optical fiber and
dispersion-compensating optical fiber, and a
dispersion-compensating module formed by winding the
dispersion-shifted optical fiber like a coil.

Background Art

15 For achieving further higher speed and larger capacity
in optical transmission systems which carry out wavelength
division multiplexing (WDM) optical transmission, it is
important that the absolute value of accumulated chromatic
dispersion be as small as possible in a wide signal wavelength
20 band. In general, since it is hard to achieve in an optical
transmission line using only one kind of optical fiber, a
plurality of kinds of optical fibers have been connected
so as to construct an optical transmission line, thereby
lowering the absolute value of accumulated chromatic
25 dispersion in the optical transmission line in a wide band.

For example, Japanese Patent Application Laid-Open No.

HEI 6-11620 discloses a technique in which a standard single-mode optical fiber (SMF) having a zero-dispersion wavelength near a wavelength of $1.3\mu\text{m}$ and a dispersion-compensating optical fiber (DCF) which
5 compensates for the chromatic dispersion of this standard single-mode optical fiber at a wavelength of 1550 nm are connected to each other, so as to reduce the absolute value of accumulated chromatic dispersion of the optical transmission line constructed by thus connected optical
10 fibers in a $1.55\text{-}\mu\text{m}$ wavelength band.

Also, U.S. Patent No. 5,838,867 discloses a technique in which a non-zero dispersion-shifted optical fiber (NZDSF) having a small positive chromatic dispersion at a wavelength of 1550 nm and a dispersion-compensating optical fiber which
15 compensates for the chromatic dispersion and dispersion slope of this dispersion-shifted optical fiber are connected to each other, so as to lower the absolute value of accumulated chromatic dispersion of the optical transmission line constructed by thus connected optical fibers in a $1.55\text{-}\mu\text{m}$ wavelength band.
20

Here, the chromatic dispersion of a standard single-mode optical fiber (SMF) at a wavelength of 1550 nm is referred to as D_{SMF} , and its dispersion slope is referred to as S_{SMF} . The chromatic dispersion of a non-zero
25 dispersion-shifted optical fiber (NZDSF) at a wavelength of 1550 nm is referred to as D_{DSF} , and its dispersion slope

is referred to as S_{DSF} . The chromatic dispersion of a dispersion-compensating optical fiber (DCF) at a wavelength of 1550 nm is referred to as D_{DCF} , and its dispersion slope is referred to as S_{DCF} . Then, for reducing the absolute value of accumulated chromatic dispersion of an optical transmission line in a wide band including a wavelength of 1550 nm, it is required in a dispersion-compensating optical fiber (hereinafter referred to as "dispersion-compensating optical fiber for SMF") for compensating for both of the chromatic dispersion and dispersion slope of the single-mode optical fiber that its ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} be substantially equal to the ratio (S_{SMF}/D_{SMF}) of dispersion slope S_{SMF} to the chromatic dispersion D_{SMF} of the single-mode optical fiber. Also, it is required in a dispersion-compensating optical fiber (hereinafter referred to as "dispersion-compensating optical fiber for DSF") for compensating for both of the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber that its ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} be substantially equal to the ratio (S_{DSF}/D_{DSF}) of dispersion slope S_{DSF} to the chromatic dispersion D_{DSF} of the dispersion-shifted optical fiber.

Disclosure of the Invention

The inventors have studied conventional optical transmission lines in detail and, as a result, have found

problems as follows.

As compared with standard single-mode optical fibers, dispersion-shifted optical fibers have a greater ratio (S_{DSF}/D_{DSF}) at a wavelength of 1550 nm. Therefore, it is
5 necessary for dispersion-compensating optical fibers for DSF to have a greater ratio (S_{DSF}/D_{DSF}) at the wavelength of 1550 nm as compared with dispersion-compensating optical fibers for SMF.

The dispersion-compensating optical fiber for SMF
10 disclosed in Japanese Patent Application Laid-Open No. HEI 6-11620 compensates for the chromatic dispersion of a standard single-mode optical fiber having a zero-dispersion wavelength near a wavelength of $1.3\mu\text{m}$ and a large chromatic dispersion at a wavelength of 1550 nm, and has a negative
15 chromatic dispersion with a large absolute value. Therefore, this dispersion-compensating optical fiber for SMF is suitable for compensating for the chromatic dispersion of the standard single-mode optical fiber. However, this dispersion-compensating optical fiber for SMF is not
20 sufficient for compensating for the dispersion slope.

On the other hand, the dispersion-compensating optical fiber for DSF disclosed in U.S. Patent No. 5,838,867 can compensate for both of the chromatic dispersion and dispersion slope of a non-zero dispersion-shifted optical
25 fiber having a small positive chromatic dispersion at a wavelength of 1550 nm. Since this dispersion-compensating

optical fiber for DSF has a chromatic dispersion with a small absolute value, a long dispersion-compensating optical fiber for DSF is needed for compensating for both of the chromatic dispersion and dispersion slope of the non-zero dispersion-shifted optical fiber.

For example, the non-zero dispersion-shifted optical fiber disclosed in the document 1, S. Bigo, et al., "1.5 Terabit/s WDM transmission of 150 channels at 10 Gbit/s over 4 x 100 km of TeraLightTM fibre," ECOC'99, PD (1999), has a chromatic dispersion of +8 ps/nm/km and a dispersion slope of +0.06 ps/nm²/km at a wavelength of 1550 nm. On the other hand, the non-zero dispersion-shifted optical fiber disclosed in the document 2, D.W. Peckham, et al., "Reduced dispersion slope, non-zero dispersion fiber," ECOC'98, pp. 139-140 (1998), has a chromatic dispersion of +4 ps/nm/km and a dispersion slope of +0.046 ps/nm²/km at a wavelength of 1550 nm. For compensating for both of the chromatic dispersion and dispersion slope of any of the non-zero dispersion-shifted optical fibers disclosed in these documents having a length of 80 km, a dispersion-compensating optical fiber for DSF having a length of 8 km to 16 km is necessary.

Meanwhile, even upon slight bending, fundamental-mode light is likely to leak out from dispersion-compensating optical fibers for DSF in general, so that bending loss is large in the fundamental-mode light. Consequently,

transmission loss becomes greater when a dispersion-compensating optical fiber for DSF is laid as being cabled or is formed into a dispersion-compensating module as being wound like a coil. Therefore, in an optical transmission system which carries out optical communications by propagation of signals through an optical transmission line constructed by a dispersion-shifted optical fiber and a dispersion-compensating optical fiber for DSF which are connected to each other, transmission loss is so large in the optical transmission line that its repeater section cannot be elongated, whereby higher speed and larger capacity cannot further be achieved in optical communications.

In order to overcome the problems mentioned above, it is an object of the present invention to provide a dispersion-compensating optical fiber which can compensate for the chromatic dispersion and dispersion slope of a non-zero dispersion-shifted optical fiber by a short length, an optical transmission line with a low transmission loss including the dispersion-shifted optical fiber and dispersion-compensating optical fiber, and a dispersion-compensating module with a low transmission loss in which the dispersion-compensating optical fiber is wound like a coil.

The dispersion-compensating optical fiber according to the present invention has, at a wavelength of 1550 nm, a chromatic dispersion D_{DCF} of -40 ps/nm/km or less and a

ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of 0.005/nm or more. By this structure, the occurrence of non-linear phenomenon can be effectively prevented because an effective area can be easily expand.

5 Preferably, in the dispersion-compensating optical fiber according to the present invention, the chromatic dispersion D_{DCF} is -100 ps/nm/km or more but -40 ps/nm/km or less, and the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is 0.005/nm or more but 0.015/nm or less.

10 Since the chromatic dispersion D_{DCF} is negative with a large absolute value, and the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to chromatic dispersion D_{DCF} lies within the numerical range mentioned above, this dispersion-compensating optical fiber can compensate for the chromatic dispersion and

15 dispersion slope of a dispersion-shifted optical fiber in a wide band including a wavelength of 1550 nm by a short length.

The dispersion-compensating optical fiber according to the present invention preferably has an effective area

20 of $16\mu\text{m}^2$, more preferably $20\mu\text{m}^2$ or more at the wavelength of 1550 nm. In this case, it can restrain four-wave mixing from occurring and suppress deterioration in the waveforms of light signals propagating therethrough.

The dispersion-compensating optical fiber according to the present invention preferably has a cutoff wavelength

25 of $1.2\mu\text{m}$ or more but $1.8\mu\text{m}$ or less, more preferably 1.4

μm or more but $1.8\mu\text{m}$ or less. Also, the dispersion-compensating optical fiber according to the present invention preferably has a transmission loss of 0.5 dB/km or less at a wavelength of 1550 nm. In this case, bending loss can be restrained from increasing since the cutoff wavelength is longer than that conventionally obtained, and lower loss is attained even when the optical fiber is formed into a cable or module, since the transmission loss lies within the numerical range mentioned above as well.

The dispersion-shifted optical fiber according to the present invention preferably has a core region extending along a predetermined axis and having a first refractive index, and a cladding region surrounding around the outer periphery of the core region. The cladding region includes a first cladding surrounding around the outer periphery of the core region and having a second refractive index lower than the first refractive index, a second cladding surrounding around the outer periphery of the first cladding and having a third refractive index higher than the second refractive index, and a third cladding surrounding around the outer periphery of the second cladding and having a fourth refractive index lower than the third refractive index. The core region preferably has a relative refractive index difference of 0.8% or more but 2.0% or less, more preferably 0.8% or more but 1.5% or less, with reference to the fourth refractive index of the third cladding. The first cladding

preferably has a relative refractive index difference of -0.4% or lower with reference to the fourth refractive index of the third cladding. These cases are suitable for realizing a dispersion-compensating optical fiber having the above-mentioned characteristics.

In the dispersion-compensating optical fiber according to the present invention, the ratio (S_{DCF}/D_{DCF}) preferably changes by 10% or less when the outside diameter of the second cladding changes by 2%. In this case, a dispersion-compensating optical fiber having a desirable chromatic dispersion characteristic can be made easily.

On the other hand, for reduction of a transmission loss by shortening a fiber length, the dispersion-compensating optical fiber according to the present invention preferably has the chromatic dispersion D_{DCF} is -250 ps/nm/km or more but -120 ps/nm/km or less, the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is 0.005/nm or more, and an effective area of $10\mu\text{m}^2$ or more but $20\mu\text{m}^2$ or less, more preferably $(20 - |D_{DCF}|/25)$ or more but $(23 - |D_{DCF}|/25)$ or less. Because it is necessary to reduce a size of the effective area at a bending weak portion where an absolute value of dispersion becomes large. Also, the dispersion-compensating optical fiber preferably has a transmission of 1.0 dB/km or less. As described above, the dispersion-compensating optical fiber has the core region, and the cladding region including the first to third cladding.

And, it is preferably that a relative refractive index difference of the core region with respect to the third cladding is 2.0% or more but 3.0% or less, and that a relative refractive index difference of the first cladding with respect to the third cladding is -0.4% or less.

The optical transmission line according to the present invention has a repeater section laid with the above-mentioned dispersion-compensating optical fiber; and a dispersion-shifted optical fiber fusion-spliced to the dispersion-compensating optical fiber. The dispersion-shifted optical fiber has, at a wavelength of 1550 nm, a chromatic dispersion of +2 ps/nm/km or more but +10 ps/nm/km or less, and a dispersion slope of +0.04 ps/nm²/km or more but +0.12 ps/nm²/km or less. When the dispersion-shifted optical fiber and the dispersion-compensating optical fiber are connected to each other with an appropriate length ratio, thus formed optical transmission line yields, on the whole, an average chromatic dispersion with a small absolute value and an average dispersion slope with a small absolute value at the wavelength of 1550 nm. As a consequence, this optical transmission line has, on the whole, an average chromatic dispersion with a small absolute value and a small average transmission loss in a wide wavelength band including a wavelength of 1550 nm.

The optical transmission line according to the present

invention preferably has, on the whole, an average chromatic dispersion with a deviation (=maximum value - minimum value) of 0.2 ps/nm/km or less in a wavelength band of 1535 nm or more but 1560 nm or less (C band). More preferably, the average chromatic dispersion on the whole has a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm or more but 1600 nm or less (C and L bands). In an optical transmission system which carries out optical communications by making signals propagate through such an optical transmission line in this case, the optical transmission line yields a low average transmission loss, the average chromatic dispersion has a small absolute value, and optical transmission with a high bit rate is possible in a wide wavelength band (including at least the C band and further the L band) including the wavelength of 1550 nm. Therefore, this optical transmission system can elongate the repeater section and achieve further higher speed and larger capacity in optical communications.

The dispersion-compensating module according to the present invention is characterized in that the above-mentioned dispersion-compensating optical fiber is wound like a coil so as to form a module. The dispersion-compensating module in which the dispersion-compensating optical fiber is formed into a module compensates for the chromatic dispersion and dispersion slope of a dispersion-shifted optical fiber laid in a repeater

section, and yields, on the whole, an average chromatic dispersion with a small absolute value and an average dispersion slope with a small absolute value at a wavelength of 1550 nm when the dispersion-shifted optical fiber and dispersion-compensating optical fiber have an appropriate length ratio therebetween. As a consequence, the whole of the dispersion-shifted optical fiber and dispersion-compensating module have an average chromatic dispersion with a smaller absolute value and a small average transmission loss in a wide wavelength band including the wavelength of 1550 nm.

The dispersion-compensating module according to the present invention preferably has a total loss of 7 dB or less in a wavelength band of 1535 nm or more but 1565 nm or less, more preferably a total loss of 7 dB or less in a wavelength band of 1535 nm or more but 1610 nm or less, when yielding a dispersion-compensating amount of -640 ps/nm at the wavelength of 1550 nm. In the dispersion-compensating module according to the present invention, the total loss is preferably 3 dB or less in the wavelength band of 1535 nm or more but 1565 nm or less, more preferably 3 dB or less in the wavelength band of 1535 nm or more but 1610 nm or less, when the dispersion-compensating amount is -320 ps/nm at the wavelength of 1550 nm. In an optical transmission system having this dispersion-compensating module, its average transmission loss is small, its average chromatic

dispersion has a small absolute value, and optical transmission with a high bit rate is possible in a wide wavelength band (wavelength band including at least the C band and further the L band) including the wavelength of 1550 nm. As a consequence, this optical transmission system can elongate the repeater section and achieve further higher speed and larger capacity in optical communications.

Further, the dispersion-compensating optical fiber according to the present invention preferably has, at a wavelength of 1550 nm, a chromatic dispersion D_{DCF} of -40 ps/nm/km or less, a ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of $0.005/\text{nm}$ or more, and an effective area of $16\mu\text{m}^2$ or more, more preferably $20\mu\text{m}^2$ or more. In a wide wavelength band including a wavelength of 1550 nm, this dispersion-compensating optical fiber not only can compensate for the chromatic dispersion and dispersion slope of a dispersion-shifted optical fiber by a short length, but also can restrain four-wave mixing from occurring and suppress deterioration in the waveforms of light signals propagating therethrough.

Still further, the dispersion-compensating optical fiber according to the present invention preferably has, at a wavelength of 1550 nm, a chromatic dispersion D_{DCF} of -40 ps/nm/km or less, a ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of $0.005/\text{nm}$ or more, and a transmission loss of 0.5 dB/km or less. This

dispersion-compensating optical fiber not only can compensate for the chromatic dispersion and dispersion slope of a dispersion-shifted optical fiber by a short length, but also yields a low loss even when formed into a cable or module.

Brief Description of the Drawings

Fig. 1 is a view showing a schematic structure of an optical transmission system including an optical transmission line according to the present invention;

Fig. 2 is a view showing a schematic structure of an optical transmission system in which a dispersion-shifted optical fiber is laid as an optical transmission line, and a dispersion-compensating optical fiber is disposed as a dispersion-compensating module within a station;

Figs. 3A and 3B are views showing a cross-sectional structure of the dispersion-compensating optical fiber according to the present invention and its refractive index profile, respectively;

Fig. 4 is a graph showing the relationship between chromatic dispersion and dispersion slope of the dispersion-compensating optical fibers according to the first to third embodiments at the wavelength of 1550 nm;

Fig. 5 is a graph showing the wavelength dependence of bending loss at a bending diameter of 140 mm of the dispersion-compensating optical fibers according to the first to third embodiments;

Fig. 6 is a graph showing the wavelength dependence of chromatic dispersion of the dispersion-compensating optical fibers according to the first to third embodiments;

Fig. 7 is a graph showing the wavelength dependence of average chromatic dispersion on the whole of each assembly in which the dispersion-compensating optical fiber according to each of the first to third embodiments and a dispersion-shifted optical fiber are fusion-spliced to each other;

Fig. 8 is a view showing a schematic structure of the dispersion-compensating module according to the present invention;

Fig. 9 is a graph showing the relationship between chromatic dispersion and dispersion slope of the dispersion-compensating optical fiber according to the fourth embodiment at the wavelength of 1550 nm;

Fig. 10 is a graph showing the wavelength dependence of bending loss at a bending diameter of 140 mm of the dispersion-compensating optical fiber according to the fourth embodiment;

Fig. 11 is a graph showing the wavelength dependence of chromatic dispersion of the dispersion-compensating optical fiber according to the fourth embodiment;

Fig. 12 is a graph showing the wavelength dependence of average chromatic dispersion on the whole of each assembly in which the dispersion-compensating optical fiber according

to the fourth embodiment and a dispersion-shifted optical fiber are fusion-spliced to each other;

Fig. 13 is a graph showing the relationship between chromatic dispersion and dispersion slope of the dispersion-compensating optical fibers according to the fifth to seventh embodiments at the wavelength of 1550 nm;

Fig. 14 is a graph showing the wavelength dependence of bending loss at a bending diameter of 140 mm of the dispersion-compensating optical fibers according to the fifth to seventh embodiments;

Fig. 15 is a graph showing the wavelength dependence of chromatic dispersion of the dispersion-compensating optical fibers according to the fifth to seventh embodiments;

Fig. 16 is a graph showing the wavelength dependence of average chromatic dispersion on the whole of each assembly in which the dispersion-compensating optical fiber according to each of the fifth to seventh embodiments and a dispersion-shifted optical fiber are fusion-spliced to each other;

Figs. 17A and 17B are views showing a cross-sectional structure of the dispersion-compensating optical fiber according to the comparative example and its refractive index profile, respectively; and

Fig. 18 is a graph showing the relationship between chromatic dispersion and dispersion slope of the dispersion-compensating optical fiber according to the

comparative example at the wavelength of 1550 nm.

Best Modes for Carrying Out the Invention

In the following, modes for carrying out the present invention will be explained in detail with reference to the accompanying drawings. In the explanation of the drawings, constituents identical to each other will be referred to with numerals identical to each other without repeating their overlapping descriptions.

Fig. 1 is a view showing a schematic structure of an optical transmission system including an optical transmission line 30 according to the present invention. In this optical transmission system 1, the optical transmission line 30 is laid in a repeater section between a station (transmitter station or repeater station) 10 and a station (receiver station or repeater station) 20. The optical transmission line 30 is constructed by a dispersion-shifted optical fiber 31 and a dispersion-compensating optical fiber 32 which are fusion-spliced to each other. In this optical transmission system 1, signals having a plurality of wavelengths in a 1.55- μ m wavelength band sent out from the station 10 reaches the station 20 by way of the dispersion-shifted optical fiber 31 and dispersion-compensating optical fiber 32 in succession, and is received by the station 20 or is optically amplified by the station 20 so as to be further sent out to the downstream thereof.

The dispersion-shifted optical fiber 31 is a silica-based optical fiber having a small positive chromatic dispersion at a wavelength of 1550 nm. In the dispersion-shifted optical fiber 31, at the wavelength of 1550 nm, chromatic dispersion D_{DSF} is +2 ps/nm/km to +10 ps/nm/km, dispersion slope S_{DSF} is +0.04 ps/nm²/km to +0.12 ps/nm²/km, and transmission loss is about 0.20 dB/km.

The dispersion-compensating optical fiber 32 according to the present invention is a silica-based optical fiber which compensates for the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber 31 at the wavelength of 1550 nm. In the dispersion-compensating optical fiber 32, at the wavelength of 1550 nm, its chromatic dispersion D_{DCF} is -40 ps/nm/km or less, and the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is 0.005/nm or more. Preferably, in the dispersion-compensating optical fiber 32, at the wavelength of 1550 nm, the chromatic dispersion D_{DCF} is -100 ps/nm/km to -40 ps/nm/km, and the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is 0.005/nm to 0.015/nm. Also, the dispersion-compensating optical fiber 32 has an effective area of 16 μm^2 or more, preferably 20 μm^2 or more at the wavelength of 1550 nm, a cutoff wavelength of 1.2 μm to 1.8 μm , preferably 1.4 μm to 1.8 μm , and a transmission loss of 0.5 dB/km or less at the wavelength of 1550 nm.

Further, the dispersion-compensating optical fiber 32 may have, at the wavelength of 1550 nm, the chromatic dispersion D_{DCF} is -250 ps/nm/km to -120 ps/nm/km, the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is 0.005/nm or more, and an effective area of $10\mu\text{m}^2$ to $20\mu\text{m}^2$ at the wavelength of 1550 nm. Also, the dispersion-compensating optical fiber has a cutoff wavelength of $1.2\mu\text{m}$ to $1.8\mu\text{m}$, preferably $1.4\mu\text{m}$ to $1.8\mu\text{m}$, and a transmission loss of 1.0 dB/km or less at the wavelength of 1550 nm.

Since the chromatic dispersion D_{DCF} and dispersion slope S_{DCF} lie within their numerical ranges mentioned above, the dispersion-compensating optical fiber 32 having such characteristics can compensate for the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber 31 in a wide band including the wavelength of 1550 nm by a short length. Also, since the dispersion-compensating optical fiber 32 has a chromatic dispersion within the numerical range thereof mentioned above and a sufficient effective area, it can restrain four-wave mixing from occurring and suppress deterioration in the waveforms of signals propagating therethrough. Further, in the dispersion-compensating optical fiber 32, bending loss can be restrained from increasing since the cutoff wavelength lies within its numerical range mentioned above, and the optical transmission line 30 attains a lower loss even when

formed into a cable, since the transmission loss lies within the numerical range thereof mentioned above as well.

The optical transmission line 30 in which the dispersion-shifted optical fiber 31 and the dispersion-compensating optical fiber 32 are fusion-spliced to each other at an appropriate length ratio has, on the whole, an average chromatic dispersion with a small absolute value and an average dispersion slope with a small absolute value at the wavelength of 1550 nm. As a consequence, the optical transmission line 30 has, on the whole, an average chromatic dispersion with a smaller absolute value in a wide band including the wavelength of 1550 nm. Also, the optical transmission line 30 has a small average transmission loss as a whole. The deviation of the average chromatic dispersion of the whole optical transmission line 30 is preferably 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1560 nm (C band), more preferably 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1600 nm (C and L bands). In the optical transmission system 1, which carries out optical communications by making signals propagating through the optical transmission line 30, the average transmission loss of the optical transmission line 30 is small, the absolute value of average chromatic dispersion is small, and optical transmission with a high bit rate is possible in a wide wavelength band (including at least the C band and further the L band) including the wavelength of 1550 nm. Therefore,

the optical transmission system 1 can elongate the repeater section and achieve further higher speed and larger capacity in optical communications.

Fig. 2 is a view showing a schematic structure of an optical transmission system 2 in which a dispersion-shifted optical fiber 31 is laid as an optical transmission line, and a dispersion-compensating optical fiber 32 is disposed as a dispersion-compensating module within a station 20. In this optical transmission system 2, the dispersion-shifted optical fiber 31 is laid as an optical transmission line in a repeater section between a station (transmitter station or repeater station) 10 and the station (receiver station or repeater station) 20. In the optical transmission system 2, signals having a plurality of wavelengths in a 1.55- μ m wavelength band sent out from the station 10 reach the station 20 by way of the dispersion-shifted optical fiber 31 acting as the optical transmission line. In the station 20, the signals are optically amplified by an optical amplifier 21, their dispersion is compensated for by the dispersion-compensating optical fiber 32, and the signals are optically amplified by an optical amplifier 22 and then is received or further sent out to the downstream thereof.

The dispersion-shifted optical fiber 31 employed as an optical transmission line in the optical transmission system 2 of Fig. 2 has characteristics similar to those of the dispersion-shifted optical fiber 31 used as a part of

the optical transmission line in the optical transmission system 1 of Fig. 1. Also, the dispersion-compensating optical fiber 32 employed as a dispersion-compensating module in the optical transmission system 2 of Fig. 2 has characteristics similar to those of the dispersion-compensating module 32 used as a part of the optical transmission line in the optical transmission system 1 of Fig. 1. In the optical transmission system 2 shown in Fig. 2, however, the dispersion-compensating optical fiber 32 is disposed within the station 20 as being wound like a coil about a bobbin so as to form a module.

Since the chromatic dispersion D_{DCF} and dispersion slope S_{DCF} lie within their numerical ranges mentioned above, the dispersion-compensating optical fiber 32 having the above-mentioned characteristics can compensate for the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber 31 in a wide band including the wavelength of 1550 nm by a short length. Also, since the dispersion-compensating optical fiber 32 has a chromatic dispersion within the numerical range thereof mentioned above and a sufficient effective area, it can restrain four-wave mixing from occurring and suppress deterioration in the waveforms of signals propagating therethrough. Further, the dispersion-compensating optical fiber 32 can restrain bending loss from increasing since the cutoff wavelength lies within its numerical range mentioned above, and attains

a lower loss even when formed into a module, since the transmission loss lies within the numerical range thereof mentioned above as well.

5 The whole of the dispersion-shifted optical fiber 31 as an optical transmission line and the dispersion-compensating optical fiber 32 as a dispersion-compensating module has, on the whole, an average chromatic dispersion with a small absolute value and an average dispersion slope with a small absolute value at the
10 wavelength of 1550 nm when they have their respective appropriate lengths. As a consequence, the whole of the dispersion-shifted optical fiber 31 and dispersion-compensating optical fiber 32 has an average chromatic dispersion with a smaller absolute value in a wide
15 band including the wavelength of 1550 nm, and a small average transmission loss. The deviation of their total average chromatic dispersion is preferably 0.2 ps/nm/km or less in the wavelength band of 1535 nm to 1560 nm (C band), more preferably 0.2 ps/nm/km or less in the wavelength band of
20 1535 nm to 1600 nm (C and L bands).

On the other hand, the dispersion-compensating optical fiber 32 as a dispersion-compensating module preferably has a total loss of 7 dB or less in the wavelength band of 1535 nm to 1565 nm (C band), more preferably a total loss of 7
25 dB or less in the wavelength band of 1535 nm to 1610 nm (C and L bands), when yielding a dispersion-compensating amount

of -640 ps/nm at the wavelength of 1550 nm. Also, the dispersion-compensating optical fiber 32 as a dispersion-compensating module preferably has a total loss of 3 dB or less in the wavelength band of 1535 nm to 1565 nm (C band), more preferably a total loss of 3 dB or less in the wavelength band of 1535 nm to 1610 nm (C and L bands), when yielding a dispersion-compensating amount of -320 ps/nm at the wavelength of 1550 nm.

In the optical transmission system 2, the average transmission loss is small, the absolute value of average chromatic dispersion is small, and optical transmission with a high bit rate is possible in a wide wavelength band (including at least the C band and further the L band) including the wavelength of 1550 nm. Therefore, the optical transmission system 2 can elongate the repeater section and achieve further higher speed and larger capacity in optical communications.

Figs. 3A and 3B are views showing a cross-sectional structure of a dispersion-compensating optical fiber according to the present invention and its refractive index profile, respectively.

The optical fiber 100 shown in Fig. 3A corresponds to the dispersion-compensating optical fiber 32, and comprises a core region 110 extending along a predetermined axis and a cladding region 120 provided so as to surround the outer periphery of the core region 110. The core region 110 has a refractive index n_1 and an outer diameter of $2a$. Further,

the cladding region 120 comprises a first cladding 121 having a second refractive index n_2 ($< n_1$) and an outside diameter 2b, a second cladding 122 provided so as to surround the outer periphery of the first cladding 121, having a third refractive index n_3 ($> n_2$, $< n_1$) and an outside diameter 2c, and a third cladding 123 provided so as to surround the outer periphery of the second cladding 122, having a fourth refractive index n_4 ($< n_3$, $> n_2$).

The refractive index profile 150 shown in Fig. 3B indicates respective refractive indices at individual parts on the line L1 in Fig. 3A, such that areas 151, 152, 153, and 154 in the refractive index profile 150 represent refractive indices of individual parts on the line L1 in the core region 110, first cladding 121, second cladding 122, and third cladding 123, respectively.

In the dispersion-compensating optical fiber 100 of Figs. 3A and 3B, with respect to the third cladding 123 acting as a reference region, the relative refractive index difference Δn_1 of the core region 110, the relative refractive index difference Δn_2 of first cladding 121, and the relative refractive index difference Δn_3 of second cladding 122 are given by the following respective expressions:

$$\Delta n_1 = (n_1 - n_4) / n_4$$

$$\Delta n_2 = (n_2 - n_4) / n_4$$

$$\Delta n_3 = (n_3 - n_4) / n_4$$

where n_1 is the refractive index of the core region 110, n_2

is the refractive index of the first cladding 121, n_3 is the refractive index of the second cladding 122, and n_4 is the refractive index of the third cladding 123 acting as the reference region. In this specification, the relative refractive index difference of each part is expressed in terms of percentage, and individual parameters in the above-mentioned expressions may be placed in the fixed order. Therefore, the relative refractive index difference of a glass region having a refractive index lower than that of the third cladding 123 (reference region) is expressed by a negative value.

Here, in the dispersion-compensating optical fiber 100, with reference to the refractive index n_4 of the third cladding 123, the core region 110 has a relative refractive index difference Δn_1 of 0.8% to 2.0%, more preferably 0.8% to 1.5%, the first cladding 121 has a relative refractive index difference Δn_2 of -0.4% or lower.

Since the dispersion-compensating optical fiber 100 has such a refractive index profile, its chromatic dispersion D_{DCF} , ratio (S_{DCF}/D_{DCF}), effective area, cutoff wavelength, and transmission loss lie within the respective numerical ranges mentioned above. For the dispersion-compensating optical fiber 100 having such a refractive index profile, it is preferred that silica glass be employed as a base, its core region 110 be doped with GeO_2 , its first cladding 121 be doped with F element, and its second cladding 122

be doped with GeO_2 . As a consequence, the refractive index profile shown in Fig. 3B can be realized, and the transmission loss of the dispersion-compensating optical fiber 100 at the wavelength of 1550 nm can be lowered.

5 Next, embodiments of the dispersion-compensating optical fiber 32 according to the present invention will now be explained. Each of the dispersion-compensating optical fibers DCF1-DCF7 respectively according to a first to seventh embodiments, which will be explained in the following, has a sectional-structure of Fig. 3A and a refractive index profile 150 of Fig. 3B.

First Embodiment

15 In the dispersion-compensating optical fiber DCF1 according to the first embodiment, with respect to the third cladding 123, the relative refractive index difference Δn_1 of the core region 110 was 1.2%, the relative refractive index difference Δn_2 of the first cladding 121 was -0.50%, the relative refractive index difference Δn_3 of the second cladding 122 was 0.20%, the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding 122 was 0.30, and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122 was 0.60. When the outside diameter $2c$ of the second cladding 122 was $17.7\mu\text{m}$, at the wavelength of 1550 nm, the dispersion-compensating optical fiber DCF1 of the first embodiment exhibited a chromatic dispersion D_{DCF} of -62.4

ps/nm/km, a dispersion slope S_{DCF} of -0.44 ps/nm²/km, an effective area of $24.4\mu\text{m}^2$, a bending loss of 10 dB/m at a bending diameter of 20 mm, and a transmission loss of 0.30 dB/km. Also, its cutoff wavelength was 1224 nm, and the ratio
5 (S_{DCF}/D_{DCF}) at the wavelength of 1550 nm was 0.0071/nm.

Second Embodiment

In the dispersion-compensating optical fiber DCF2 according to the second embodiment, with respect to the third cladding 123, the relative refractive index difference Δ
10 n_1 of the core region 110 was 1.3%, the relative refractive index difference Δn_2 of the first cladding 121 was -0.50% , the relative refractive index difference Δn_3 of the second cladding 122 was 0.23% , the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding
15 122 was 0.27, and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122 was 0.55. When the outside diameter $2c$ of the second cladding 122 was $19.0\mu\text{m}$, at the wavelength of 1550 nm, the dispersion-compensating optical fiber DCF2 of the second
20 embodiment exhibited a chromatic dispersion D_{DCF} of -80.4 ps/nm/km, a dispersion slope S_{DCF} of -0.59 ps/nm²/km, an effective area of $23.9\mu\text{m}^2$, a bending loss of 4 dB/m at a bending diameter of 20 mm, a transmission loss of 0.33 dB/km. Also, its cutoff wavelength was 1576 nm, and the ratio
25 (S_{DCF}/D_{DCF}) at the wavelength of 1550 nm was 0.0073/nm.

Third Embodiment

In the dispersion-compensating optical fiber DCF3 according to the third embodiment, with respect to the third cladding 123, the relative refractive index difference Δn_1 of the core region 110 was 1.7%, the relative refractive index difference Δn_2 of the first cladding 121 was -0.50%, the relative refractive index difference Δn_3 of the second cladding 122 was 0.25%, the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding 122 was 0.23, and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122 was 0.53. When the outside diameter $2c$ of the second cladding 122 was $18.7\mu\text{m}$, at the wavelength of 1550 nm, the dispersion-compensating optical fiber DCF3 of the third embodiment exhibited a chromatic dispersion D_{DCF} of -83.7 ps/nm/km, a dispersion slope S_{DCF} of -0.66 ps/nm²/km, an effective area of $17.2\mu\text{m}^2$, a bending loss of 0.2 dB/m at a bending diameter of 20 mm, a transmission loss of 0.39 dB/km. Also, its cutoff wavelength was 1696 nm, and the ratio $(S_{\text{DCF}}/D_{\text{DCF}})$ at the wavelength of 1550 nm was 0.0079/nm.

Fig. 4 is a graph showing a relationship between chromatic dispersion and dispersion slope in each dispersion-compensating optical fiber of the first to third embodiments at the wavelength of 1550 nm. In Fig. 4, G110 indicates a curve for the first embodiment, G210 indicates a curve for the second embodiment, and G310 indicates a curve

for the third embodiment. Shown here is the relationship between chromatic dispersion D_{DCF} and dispersion slope S_{DCF} in each dispersion-compensating optical fiber of these embodiments when the outside diameter $2c$ of the second cladding 122 is changed. As can be seen from the graph of Fig. 4, the change in the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is small in each of the dispersion-compensating optical fibers DCF1 to DCF3 if the chromatic dispersion D_{DCF} is approximately within the range of -60 ps/nm/km to -10 ps/nm/km even when the outside diameter $2c$ of the second cladding 122 changes. In the dispersion-compensating optical fiber DCF1 of the first embodiment, the ratio (S_{DCF}/D_{DCF}) changes by 2.5% or less when the outside diameter $2c$ of the second cladding 122 changes by 2%, and further the range of the chromatic dispersion D_{DCF} where the ratio (S_{DCF}/D_{DCF}) is kept to be 10% or less is -68 ps/nm/km to -17 ps/nm/km. In the dispersion-compensating optical fiber DCF2 of the second embodiment, the ratio (S_{DCF}/D_{DCF}) changes by 9.0% or less when the outside diameter $2c$ of the second cladding 122 changes by 2%, and further the range of the chromatic dispersion D_{DCF} where the ratio (S_{DCF}/D_{DCF}) is kept to be 10% or less is -81 ps/nm/km to -30 ps/nm/km. In the dispersion-compensating optical fiber DCF3 of the third embodiment, the ratio (S_{DCF}/D_{DCF}) changes by 4.0% or less when the outside diameter $2c$ of the second cladding 122 changes

by 2%, and further the range of the chromatic dispersion D_{DCF} where the ratio (S_{DCF}/D_{DCF}) is kept to be 10% or less is -115 ps/nm/km to -62 ps/nm/km. If the change in ratio (S_{DCF}/D_{DCF}) is 10% or less when the outside diameter $2c$ of the second cladding 122 changes by 2% as such, then a dispersion-compensating optical fiber having a desirable chromatic dispersion characteristic can easily be made.

Fig. 5 is a graph showing the wavelength dependence of bending loss in each dispersion-compensating optical fiber of the first to third embodiments at a bending diameter of 140 mm. In Fig. 5, G120 indicates a curve for the first embodiment, G220 indicates a curve for the second embodiment, and G320 indicates a curve for the third embodiment. The outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF1 of the first embodiment was $17.7\mu\text{m}$, the outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF2 of the second embodiment was $19.0\mu\text{m}$, and the outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF3 of the third embodiment was $18.7\mu\text{m}$. As can be seen from the graph of Fig. 5, each of the dispersion-compensating optical fibers DCF1 to DCF3 has a low bending loss in the range where wavelength is 1610 nm or shorter.

Therefore, each of the dispersion-compensating optical fibers DCF1 to DCF3 is not only suitably employable

as the dispersion-compensating optical fiber 32 constituting a part of the optical transmission line 30 in the optical transmission system 1 shown in Fig. 1, but also is suitably employable as the dispersion-compensating optical fiber 32 forming a dispersion-compensating module in the optical transmission system 2 shown in Fig. 2, thereby being able to compensate for chromatic dispersion not only in the C band but also in the L band with a low loss.

Fig. 6 is a graph showing the wavelength dependence of chromatic dispersion in each dispersion-compensating optical fiber of the first to third embodiments. In Fig. 6, G130 indicates a curve for the first embodiment, G230 indicates a curve for the second embodiment, G330 indicates a curve for the third embodiment, and G1000 indicates a curve for a non-zero dispersion-shifted optical fiber NZDSF disclosed in the above-mentioned document 1. Here, the outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF1 of the first embodiment was $17.7\mu\text{m}$, the outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF2 of the second embodiment was $19.0\mu\text{m}$, and the outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF3 of the third embodiment was $18.7\mu\text{m}$, too.

Fig. 7 is a graph showing the wavelength dependence of the average chromatic dispersion on the whole, in each

assembly made by each dispersion-compensating optical fiber of the first to third embodiments and the dispersion-shifted optical fiber connected to each other. In Fig. 7, G140 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF1 of the first embodiment and the dispersion-shifted optical fiber NZDSF of Fig. 6 were connected to each other, G240 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF2 of the second embodiment and the dispersion-shifted optical fiber NZDSF of Fig. 6 were connected to each other, and G340 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF3 of the third embodiment and the dispersion-shifted optical fiber NZDSF of Fig. 6 were connected to each other. For compensating for the chromatic dispersion at the wavelength of 1550 nm of the dispersion-shifted optical fiber NZDSF having the chromatic dispersion characteristic shown in Fig. 6 and a length of 80 km, a length of 10.3 km was necessary for the dispersion-compensating optical fiber DCF1 of the first embodiment, a length of 8.0 km was necessary for the dispersion-compensating optical fiber DCF2 of the second embodiment, and a length of 7.5 km was necessary for the dispersion-compensating optical fiber DCF3 of the third embodiment.

In the assembly in which the dispersion-compensating optical fiber DSF1 of the first embodiment and the

dispersion-shifted optical fiber NZDSF were connected to each other, the total average chromatic dispersion had a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1600 nm (C and L bands). In the assembly in which
5 the dispersion-compensating optical fiber DSF2 of the second embodiment and the dispersion-shifted optical fiber NZDSF were connected to each other, the average chromatic dispersion on the whole had a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1560 nm (C band).
10 Further, in the assembly in which the dispersion-compensating optical fiber DSF3 of the third embodiment and the dispersion-shifted optical fiber NZDSF were connected to each other, the average chromatic dispersion on the whole had a deviation of 0.2 ps/nm/km or less in a wavelength band
15 of 1535 nm to 1560 nm (C band). As a consequence, they are capable of optical transmission over a distance of 400 km at a bit rate of 40 Gb/s.

Fig. 8 is a view showing a schematic structure of a dispersion-compensating module including the
20 dispersion-compensating optical fiber according to the present invention. The dispersion-compensating optical fiber 100 (corresponding to the dispersion-compensating optical fiber 32) is accommodated in the case 300 with input- and output- connectors 310. Two ends of the fiber 100 are
25 respectively fusion-spliced to pigtail fibers 320 to reduce connection loss. When the dispersion-compensating optical

fiber DCF1 of the first embodiment having a length of 10.3 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 4.1 dB (at the wavelength of 1550 nm). When the dispersion-compensating optical fiber DCF2 of the second embodiment having a length of 8.0 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 4.4 dB (at the wavelength of 1550 nm). Further, when the dispersion-compensating optical fiber DCF3 of the third embodiment having a length of 7.5 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 4.1 dB (at the wavelength of 1550 nm).

Also, when the dispersion-compensating optical fiber DCF1 of the first embodiment was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, while the dispersion-compensating amount at the wavelength of 1550 nm was -320 ps/nm, the total loss was 2.3 dB (at the wavelength of 1550 nm). When the dispersion-compensating optical fiber DCF2 of the second embodiment was wound at a bending diameter of 140 mm so as

to form a dispersion-compensating module, while the dispersion-compensating amount at a wavelength of 1550 nm was -320 ps/nm, the total loss was 2.5 dB (at the wavelength of 1550 nm). Further, when the dispersion-compensating optical fiber DCF3 of the third embodiment was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, while the dispersion-compensating amount at a wavelength of 1550 nm was -320 ps/nm, the total loss was 2.7 dB (at the wavelength of 1550 nm).

Thus, each of the dispersion-compensating optical fibers DCF1 to DCF3 can compensate for the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber NZDSF by a short length with a low loss in a wide wavelength band including the wavelength of 1550 nm.

Fourth Embodiment

In the dispersion-compensating optical fiber DCF4 according to the fourth embodiment, with respect to the third cladding 123, the relative refractive index difference Δn_1 of the core region 110 was 1.6%, the relative refractive index difference Δn_2 of the first cladding 121 was -0.50%, the relative refractive index difference Δn_3 of the second cladding 122 was 0.24%, the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding 122 was 0.23, and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122

was 0.55. When the outside diameter $2c$ of the second cladding 122 was $19.2\mu\text{m}$, at the wavelength of 1550 nm, the dispersion-compensating optical fiber DCF4 of the fourth embodiment exhibited a chromatic dispersion D_{DCF} of -85.1 ps/nm/km, a dispersion slope S_{DCF} of -0.83 ps/nm²/km, an effective area of $18.1\mu\text{m}^2$, a bending loss of 0.9 dB/m at a bending diameter of 20 mm, a transmission loss of 0.38 dB/km. Also, its cutoff wavelength was 1638 nm, and the ratio ($S_{\text{DCF}}/D_{\text{DCF}}$) at the wavelength of 1550 nm was 0.0098/nm.

Fig. 9 is a graph showing a relationship between chromatic dispersion and dispersion slope in the dispersion-compensating optical fiber of the fourth embodiment at the wavelength of 1550 nm. In Fig. 9, G410 indicates a curve for the fourth embodiment. Shown here is the relationship between chromatic dispersion D_{DCF} and dispersion slope S_{DCF} in the dispersion-compensating optical fiber of this embodiment when the outside diameter $2c$ of the second cladding 122 is changed. As can be seen from the graph of Fig. 9, the change in the ratio ($S_{\text{DCF}}/D_{\text{DCF}}$) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is kept to be 10% or less in the dispersion-compensating optical fibers DCF4 if the chromatic dispersion D_{DCF} is approximately within the range of -102 ps/nm/km to -71 ps/nm/km even when the outside diameter $2c$ of the second cladding 122 changes. In the dispersion-compensating optical fiber DCF4 of the fourth embodiment, the ratio ($S_{\text{DCF}}/D_{\text{DCF}}$) changes by 5.8% or less when

the outside diameter $2c$ of the second cladding 122 changes by 2%. If the change in ratio (S_{DCF}/D_{DCF}) is 10% or less when the outside diameter $2c$ of the second cladding 122 changes by 2% as such, then a dispersion-compensating optical fiber having a desirable chromatic dispersion characteristic can easily be made.

Fig. 10 is a graph showing the wavelength dependence of bending loss in the dispersion-compensating optical fiber of the fourth embodiment at a bending diameter of 140 mm. In Fig. 5, G420 indicates a curve for the fourth embodiment. The outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF4 of the fourth embodiment was $17.2\mu\text{m}$. As can be seen from the graph of Fig. 10, the dispersion-compensating optical fibers DCF4 has a low bending loss in the range where wavelength is 1610 nm or shorter.

Therefore, the dispersion-compensating optical fibers DCF4 is not only suitably employable as the dispersion-compensating optical fiber 32 constituting a part of the optical transmission line 30 in the optical transmission system 1 shown in Fig. 1, but also is suitably employable as the dispersion-compensating optical fiber 32 forming a dispersion-compensating module in the optical transmission system 2 shown in Fig. 2, thereby being able to compensate for chromatic dispersion not only in the C band but also in the L band with a low loss.

Fig. 11 is a graph showing the wavelength dependence of chromatic dispersion in the dispersion-compensating optical fiber of the fourth embodiment. In Fig. 11, G430 indicates a curve for the fourth embodiment, and G1000 indicates a curve for a non-zero dispersion-shifted optical fiber NZDSF disclosed in the above-mentioned document 1, having a dispersion of 4 ps/nm/km or less and a dispersion slope of 0.046 ps/nm²/km or less. Here, the outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF4 of the fourth embodiment was 19.2 μ m, too.

Fig. 12 is a graph showing the wavelength dependence of the average chromatic dispersion on the whole, in the assembly made by the dispersion-compensating optical fiber of the fourth embodiment and the dispersion-shifted optical fiber connected to each other. In Fig. 12, G440 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF4 of the fourth embodiment and the dispersion-shifted optical fiber NZDSF of Fig. 11 were connected to each other. For compensating for the chromatic dispersion at the wavelength of 1550 nm of the dispersion-shifted optical fiber NZDSF having the chromatic dispersion characteristic shown in Fig. 11 and a length of 80 km, a length of 10.3 km was necessary for the dispersion-compensating optical fiber DCF1 of the first embodiment, a length of 4.4 km was necessary for the dispersion-compensating optical fiber DCF4 of the fourth

embodiment.

In the assembly in which the dispersion-compensating optical fiber DSF4 of the fourth embodiment and the dispersion-shifted optical fiber NZDSF were connected to each other, the total average chromatic dispersion had a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1600 nm (C and L bands). As a consequence, they are capable of optical transmission over a repeater distance of 400 km at a bit rate of 40 Gb/s.

When the dispersion-compensating optical fiber DCF4 of the fourth embodiment having a length of 4.4 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 3.9 dB (at the wavelength of 1550 nm). Also, when the dispersion-compensating optical fiber DCF4 of the fourth embodiment was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, while the dispersion-compensating amount at the wavelength of 1550 nm was -320 ps/nm, the total loss was 2.5 dB (at the wavelength of 1550 nm).

Thus, the dispersion-compensating optical fibers DCF4 can compensate for the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber NZDSF by a short length with a low loss in a wide wavelength band including

the wavelength of 1550 nm.

Fifth Embodiment

In the dispersion-compensating optical fiber DCF5 according to the fifth embodiment, with respect to the third
5 cladding 123, the relative refractive index difference Δn_1 of the core region 110 was 2.1%, the relative refractive index difference Δn_2 of the first cladding 121 was -0.50%, the relative refractive index difference Δn_3 of the second
10 cladding 122 was 0.20%, the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding 122 was 0.18, and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122 was 0.49. When the outside diameter $2c$ of the second cladding 122 was $19.4\mu\text{m}$, at the wavelength of 1550 nm, the
15 dispersion-compensating optical fiber DCF5 of the fifth embodiment exhibited a chromatic dispersion D_{DCF} of -160.7 ps/nm/km; a dispersion slope S_{DCF} of -1.63 ps/nm²/km, an effective area of $15.7\mu\text{m}^2$, a bending loss of 1.8 dB/m at a bending diameter of 20 mm, a transmission loss of 0.49
20 dB/km. Also, its cutoff wavelength was 1566 nm, and the ratio $(S_{\text{DCF}}/D_{\text{DCF}})$ at the wavelength of 1550 nm was 0.0101/nm.

Sixth Embodiment

In the dispersion-compensating optical fiber DCF6 according to the sixth embodiment, with respect to the third
25 cladding 123, the relative refractive index difference Δn_1 of the core region 110 was 2.4%, the relative refractive

index difference Δn_2 of the first cladding 121 was -0.50% , the relative refractive index difference Δn_3 of the second cladding 122 was 0.40% , the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding 122 was 0.20 , and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122 was 0.65 . When the outside diameter $2c$ of the second cladding 122 was $16.0\mu\text{m}$, at the wavelength of 1550 nm , the dispersion-compensating optical fiber DCF6 of the sixth embodiment exhibited a chromatic dispersion D_{DCF} of -181.6 ps/nm/km , a dispersion slope S_{DCF} of $-1.87\text{ ps/nm}^2/\text{km}$, an effective area of $13.8\mu\text{m}^2$, a bending loss of 0.5 dB/m at a bending diameter of 20 mm , a transmission loss of 0.61 dB/km . Also, its cutoff wavelength was 1660 nm , and the ratio $(S_{\text{DCF}}/D_{\text{DCF}})$ at the wavelength of 1550 nm was $0.0103/\text{nm}$.

Seventh Embodiment

In the dispersion-compensating optical fiber DCF7 according to the seventh embodiment, with respect to the third cladding 123, the relative refractive index difference Δn_1 of the core region 110 was 2.7% , the relative refractive index difference Δn_2 of the first cladding 121 was -0.50% , the relative refractive index difference Δn_3 of the second cladding 122 was 0.40% , the ratio $(2a/2c)$ of the respective outside diameters of the core region 110 and second cladding 122 was 0.19 , and the ratio $(2b/2c)$ of the respective outside diameters of the first cladding 121 and second cladding 122

was 0.67. When the outside diameter $2c$ of the second cladding 122 was $15.2\mu\text{m}$, at the wavelength of 1550 nm, the dispersion-compensating optical fiber DCF7 of the seventh embodiment exhibited a chromatic dispersion D_{DCF} of -215.8 ps/nm/km, a dispersion slope S_{DCF} of -2.12 ps/nm²/km, an effective area of $13.1\mu\text{m}^2$, a bending loss of 1.3 dB/m at a bending diameter of 20 mm, a transmission loss of 0.75 dB/km. Also, its cutoff wavelength was 1514 nm, and the ratio ($S_{\text{DCF}}/D_{\text{DCF}}$) at the wavelength of 1550 nm was 0.0097/nm.

Fig. 13 is a graph showing a relationship between chromatic dispersion and dispersion slope in each dispersion-compensating optical fiber of the fifth to seventh embodiments at the wavelength of 1550 nm. In Fig. 13, G510 indicates a curve for the fifth embodiment, G610 indicates a curve for the sixth embodiment, and G710 indicates a curve for the seventh embodiment. Shown here is the relationship between chromatic dispersion D_{DCF} and dispersion slope S_{DCF} in each dispersion-compensating optical fiber of these embodiments when the outside diameter $2c$ of the second cladding 122 is changed. As can be seen from the graph of Fig. 13, the change in the ratio ($S_{\text{DCF}}/D_{\text{DCF}}$) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is small in each of the dispersion-compensating optical fibers DCF5 to DCF7 if the chromatic dispersion D_{DCF} is approximately within the range of -200 ps/nm/km to -120 ps/nm/km even when the outside diameter $2c$ of the second cladding 122 changes. In the

dispersion-compensating optical fiber DCF5 of the fifth embodiment, the ratio (S_{DCF}/D_{DCF}) changes by 7.7% or less when the outside diameter 2c of the second cladding 122 changes by 2%, and further the range of the chromatic dispersion D_{DCF} where the ratio (S_{DCF}/D_{DCF}) is kept to be 10% or less is -192 ps/nm/km to -135 ps/nm/km. In the dispersion-compensating optical fiber DCF6 of the sixth embodiment, the ratio (S_{DCF}/D_{DCF}) changes by 4.6% or less when the outside diameter 2c of the second cladding 122 changes by 2%, and further the range of the chromatic dispersion D_{DCF} where the ratio (S_{DCF}/D_{DCF}) is kept to be 10% or less is -226 ps/nm/km to -146 ps/nm/km. In the dispersion-compensating optical fiber DCF7 of the seventh embodiment, the ratio (S_{DCF}/D_{DCF}) changes by 4.9% or less when the outside diameter 2c of the second cladding 122 changes by 2%, and further the range of the chromatic dispersion D_{DCF} where the ratio (S_{DCF}/D_{DCF}) is kept to be 10% or less is -173 ps/nm/km to -269 ps/nm/km. If the change in ratio (S_{DCF}/D_{DCF}) is 10% or less when the outside diameter 2c of the second cladding 122 changes by 2% as such, then a dispersion-compensating optical fiber having a desirable chromatic dispersion characteristic can easily be made.

Fig. 14 is a graph showing the wavelength dependence of bending loss in each dispersion-compensating optical fiber of the fifth to seventh embodiments at a bending diameter of 140 mm. In Fig. 14, G520 indicates a curve for the fifth

embodiment, G620 indicates a curve for the sixth embodiment, and G720 indicates a curve for the seventh embodiment. The outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF5 of the fifth
5 embodiment was $19.4\mu\text{m}$, the outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF6 of the sixth embodiment was $16.0\mu\text{m}$, and the outside diameter 2c of the second cladding 122 in the dispersion-compensating optical fiber DCF7 of the seventh
10 embodiment was $15.2\mu\text{m}$. As can be seen from the graph of Fig. 14, each of the dispersion-compensating optical fibers DCF5 to DCF7 has a low bending loss in the range where wavelength is 1610 nm or shorter.

Therefore, each of the dispersion-compensating
15 optical fibers DCF5 to DCF7 is not only suitably employable as the dispersion-compensating optical fiber 32 constituting a part of the optical transmission line 30 in the optical transmission system 1 shown in Fig. 1, but also is suitably employable as the dispersion-compensating optical fiber 32
20 forming a dispersion-compensating module in the optical transmission system 2 shown in Fig. 2, thereby being able to compensate for chromatic dispersion not only in the C band but also in the L band with a low loss.

Fig. 15 is a graph showing the wavelength dependence
25 of chromatic dispersion in each dispersion-compensating optical fiber of the fifth to seventh embodiments. In Fig.

15, G530 indicates a curve for the fifth embodiment, G630 indicates a curve for the sixth embodiment, and G730 indicates a curve for the seventh embodiment. Here, the outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF5 of the fifth embodiment was $19.4\mu\text{m}$, the outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF6 of the sixth embodiment was $16.0\mu\text{m}$, and the outside diameter $2c$ of the second cladding 122 in the dispersion-compensating optical fiber DCF7 of the seventh embodiment was $15.2\mu\text{m}$, too.

Fig. 16 is a graph showing the wavelength dependence of the average chromatic dispersion on the whole, in each assembly made by each dispersion-compensating optical fiber of the fifth to seventh embodiments and a non-dispersion-shifted optical fiber, which is disclosed in the above-mentioned document 2 and has a dispersion of 4 ps/nm/km or less and a dispersion slope of $0.046\text{ ps/nm}^2/\text{km}$ or less, connected to each other. In Fig. 16, G540 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF5 of the fifth embodiment and the dispersion-shifted optical fiber NZDSF of the document 2 were connected to each other, G640 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF6 of the sixth embodiment and the dispersion-shifted optical fiber NZDSF of the document 2 were connected to each

other, and G740 indicates a curve for the assembly in which the dispersion-compensating optical fiber DCF7 of the seventh embodiment and the dispersion-shifted optical fiber NZDSF of the document 2 were connected to each other. For
5 compensating for the chromatic dispersion at the wavelength of 1550 nm of the dispersion-shifted optical fiber NZDSF having a length of 80 km, a length of 2.2 km was necessary for the dispersion-compensating optical fiber DCF5 of the fifth embodiment, a length of 1.9 km was necessary for the
10 dispersion-compensating optical fiber DCF6 of the sixth embodiment, and a length of 1.7 km was necessary for the dispersion-compensating optical fiber DCF7 of the seventh embodiment.

In the assembly in which the dispersion-compensating
15 optical fiber DSF5 of the fifth embodiment and the dispersion-shifted optical fiber NZDSF were connected to each other, the total average chromatic dispersion had a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1560 nm (C band). In the assembly in which the
20 dispersion-compensating optical fiber DSF6 of the sixth embodiment and the dispersion-shifted optical fiber NZDSF were connected to each other, the average chromatic dispersion on the whole had a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1600 nm (C and L
25 bands). Further, in the assembly in which the dispersion-compensating optical fiber DSF7 of the seventh

embodiment and the dispersion-shifted optical fiber NZDSF were connected to each other, the average chromatic dispersion on the whole had a deviation of 0.2 ps/nm/km or less in a wavelength band of 1535 nm to 1600 nm (C and L bands). As a consequence, they are capable of optical transmission over a repeater distance of 400 km at a bit rate of 40 Gb/s.

As shown in Fig. 8, when the dispersion-compensating optical fiber DCF5 of the fifth embodiment having a length of 2.2 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 3.0 dB (at the wavelength of 1550 nm). When the dispersion-compensating optical fiber DCF6 of the sixth embodiment having a length of 1.9 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 2.7 dB (at the wavelength of 1550 nm). Further, when the dispersion-compensating optical fiber DCF7 of the seventh embodiment having a length of 1.7 km was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, the dispersion-compensating amount at the wavelength of 1550 nm was -640 ps/nm, and the total loss was 2.5 dB (at the wavelength of 1550 nm).

Also, when the dispersion-compensating optical fiber DCF5 of the fifth embodiment was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, while the dispersion-compensating amount at the wavelength of 1550 nm was -320 ps/nm, the total loss was 2.0 dB (at the wavelength of 1550 nm). When the dispersion-compensating optical fiber DCF6 of the sixth embodiment was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, while the dispersion-compensating amount at a wavelength of 1550 nm was -320 ps/nm, the total loss was 1.9 dB (at the wavelength of 1550 nm). Further, when the dispersion-compensating optical fiber DCF7 of the seventh embodiment was wound at a bending diameter of 140 mm so as to form a dispersion-compensating module, while the dispersion-compensating amount at a wavelength of 1550 nm was -320 ps/nm, the total loss was 1.7 dB (at the wavelength of 1550 nm).

Thus, each of the dispersion-compensating optical fibers DCF5 to DCF7 can compensate for the chromatic dispersion and dispersion slope of the dispersion-shifted optical fiber NZDSF by a short length with a low loss in a wide wavelength band including the wavelength of 1550 nm.

Comparative Example

For comparison with the dispersion-compensating optical fiber of each of the above-mentioned first to seventh

embodiments, the dispersion-compensating optical fiber of a comparative example will now be explained. Figs. 17A and 17B are views showing a cross-sectional structure of the dispersion-compensating optical fiber according to the comparative example and its refractive index profile, respectively. This comparative example 200 comprises a core region 210 extending along a predetermined axis and a cladding region 220 provided so as to surround the outer periphery of the core region 210. The core region 210 has a refractive index n_1 and an outer diameter of $2a$. Further, the cladding region 220 comprises a first cladding 221 having a second refractive index n_2 ($< n_1$) and an outside diameter $2b$, and a second cladding 222 provided so as to surround the outer periphery of the first cladding 221, having a third refractive index n_3 ($> n_2$, $< n_1$).

The refractive index profile 250 shown in Fig. 17B indicates respective refractive indices at individual parts on the line L2 in Fig. 17A, such that areas 251, 252, and 253 in the refractive index profile 150 represent refractive indices of individual parts on the line L2 in the core region 210, first cladding 221, and second cladding 222, respectively.

In the comparative example 200 of Figs. 17A and 17B, with respect to the second cladding 222 acting as a reference region, the relative refractive index difference Δn_1 of the core region 210, and the relative refractive index difference

Δn_2 of first cladding 221 are given by the following respective expressions:

$$\Delta n_1 = (n_1 - n_3)/n_3$$

$$\Delta n_2 = (n_2 - n_3)/n_3$$

5 where n_1 is the refractive index of the core region 210, n_2 is the refractive index of the first cladding 221, and n_3 is the refractive index of the second cladding 222 acting as the reference region. In this specification, the relative refractive index difference of each part is expressed in
10 terms of percentage, and individual parameters in the above-mentioned expressions may be placed in the fixed order. Therefore, the relative refractive index difference of a glass region having a refractive index lower than that of the second cladding 222 (reference region) is expressed by
15 a negative value.

Here, in the comparative example 200, with reference to the refractive index n_3 of the second cladding 222, the core region 210 has a relative refractive index difference Δn_1 of 1.2%, the first cladding 221 has a relative refractive
20 index difference Δn_2 of -0.36%. Also, the ratio $R_a (= 2a/2b)$ of the outside diameter $2a$ of the core region 210 to the outside diameter $2b$ of the first cladding 221 is 0.50.

Fig. 18 is a graph showing the relationship between chromatic dispersion and dispersion slope of the
25 dispersion-compensating optical fiber of the comparative example at the wavelength of 1550 nm. Shown here is the

relationship between chromatic dispersion D_{DCF} and dispersion slope S_{DCF} in the comparative example when the outside diameter $2b$ of the first cladding 221 is changed. In the range where chromatic dispersion is -40 ps/nm/km or less, the comparative example has such an unfavorable bending characteristic that it cannot be used. If the outside diameter $2c$ of the second cladding 222 changes greatly, then the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} will change greatly. For example, when the outside diameter $2b$ of the first cladding 221 is $10.0\mu\text{m}$, then the chromatic dispersion D_{DCF} is -28 ps/nm/km (a condition corresponding the point A in Fig. 18), whereby the dispersion slope S_{DCF} is -0.081 ps/nm²/km. Also, when the outside diameter $2b$ of the first cladding 221 is $9.8\mu\text{m}$, then the chromatic dispersion D_{DCF} is -22 ps/nm/km (a condition corresponding the point B in Fig. 18), whereby the dispersion slope S_{DCF} is -0.056 ps/nm²/km. If the outside diameter $2b$ changes from this value by 2%, then the ratio (S_{DCF}/D_{DCF}) will change by as much as 17%. As a consequence, a dispersion-compensating optical fiber having a desirable chromatic dispersion characteristic is hard to make.

As compared with the dispersion-compensating optical fiber of the comparative example, the dispersion-compensating optical fiber according to the embodiment (including the dispersion-compensating optical fibers of the first to seventh embodiments) has excellent

bending characteristics and can also be used in the range where chromatic dispersion is -40 ps/nm/km or less as mentioned above. Also, even when the outside diameter $2c$ of the second cladding changes, the change in ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is small in the dispersion-compensating optical fiber according to the present invention if the chromatic dispersion D_{DCF} is within a predetermined range. Therefore, it is easy for the dispersion-compensating optical fiber according to the present invention to be made with desirable chromatic dispersion characteristics.

Industrial Applicability

As explained in detail in the foregoing, the dispersion-compensating optical fiber according to the present invention has, at a wavelength of 1550 nm, a chromatic dispersion D_{DCF} of -40 ps/nm/km or less (preferably -100 ps/nm/km to -40 ps/nm/km or -250 ps/nm/km to -120 ps/nm/km), a ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of 0.005 /nm or more (preferably 0.005 /nm to 0.015 /nm). Since the dispersion-compensating optical fiber according to the present invention has such characteristics, it can compensate for the chromatic dispersion and dispersion slope of a dispersion-shifted optical fiber in a wide wavelength band including the wavelength of 1550 nm by a short length.

CLAIMS

1. A dispersion-compensating optical fiber having a core region extending along a predetermined axis and a cladding region surrounding around the outer periphery of said core region, said dispersion-compensating optical fiber having, at a wavelength of 1550 nm, characteristics of:

a chromatic dispersion D_{DCF} of -40 ps/nm/km or less; and

a ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of 0.005/nm or more.

2. A dispersion-compensating optical fiber according to claim 1, wherein said dispersion-compensating optical fiber has, at the wavelength of 1550 nm, characteristics of: the chromatic dispersion D_{DCF} of -100 ps/nm/km or more but -40 ps/nm/km or less; and the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of 0.005/nm or more but 0.015/nm or less.

3. A dispersion-compensating optical fiber according to claim 1, wherein said dispersion-compensating optical fiber has an effective area of $16\mu\text{m}^2$ or more at the wavelength of 1550 nm.

4. A dispersion-compensating optical fiber according to claim 3, wherein said dispersion-compensating optical fiber has an effective area of $20\mu\text{m}^2$ or more at the wavelength of 1550 nm.

5. A dispersion-compensating optical fiber

according to claim 1, wherein said dispersion-compensating optical fiber has a cutoff wavelength of $1.2\mu\text{m}$ or more but $1.8\mu\text{m}$ or less.

5 6. A dispersion-compensating optical fiber according to claim 5, wherein said dispersion-compensating optical fiber has a cutoff wavelength of $1.4\mu\text{m}$ or more but $1.8\mu\text{m}$ or less.

10 7. A dispersion-compensating optical fiber according to claim 1, wherein said dispersion-compensating optical fiber has a transmission loss of 0.5 dB/km or less at the wavelength of 1550 nm.

 8. A dispersion-compensating optical fiber according to claim 1, wherein said core region has a first refractive index; and

15 wherein said cladding region has a first cladding surrounding around the outer periphery of said core region and having a second refractive index lower than the first refractive index, a second cladding surrounding around the outer periphery of said first cladding and having a third refractive index higher than the second refractive index, and a third cladding surrounding around the outer periphery of said second cladding and having a fourth refractive index lower than the third refractive index.

20 9. A dispersion-compensating optical fiber according to claim 8, wherein said core region has a relative refractive index difference of 0.8% or more but 2.0% or less with reference

to said third cladding.

10. A dispersion-compensating optical fiber according to claim 9, wherein said core region has a relative refractive index difference of 0.8% or more but 1.5% or less with reference to said third cladding.

11. A dispersion-compensating optical fiber according to claim 8, wherein said first cladding has a relative refractive index difference of -0.4% or less with reference to said third cladding.

12. A dispersion-compensating optical fiber according to claim 8, wherein the ratio (S_{DCF}/D_{DCF}) changes by 10% or less when an outer diameter of said second cladding changes by 2%.

13. A dispersion-compensating optical fiber according to claim 1, wherein said dispersion-compensating optical fiber has, at the wavelength of 1550 nm, characteristics of: the chromatic dispersion D_{DCF} of -250 ps/nm/km or more but -120 ps/nm/km or less; the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} of 0.005/nm or more; and an effective area of $10\mu\text{m}^2$ or more but $20\mu\text{m}^2$ or less.

14. A dispersion-compensating optical fiber according to claim 13, wherein the ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the chromatic dispersion D_{DCF} is 0.015/nm or less.

15. A dispersion-compensating optical fiber

according to claim 13, the effective area falls within a range of $(20 - |D_{DCF}|/25)$ or more but $(23 - |D_{DCF}|/25)$ or less.

16. A dispersion-compensating optical fiber according to claim 13, wherein said dispersion-compensating optical fiber has a transmission loss of 1.0 dB/km or less at the wavelength of 1550 nm.

17. A dispersion-compensating optical fiber according to claim 13, wherein said core region has a first refractive index; and

wherein said cladding region has a first cladding surrounding around the outer periphery of said core region and having a second refractive index lower than the first refractive index, a second cladding surrounding around the outer periphery of said first cladding and having a third refractive index higher than the second refractive index, and a third cladding surrounding around the outer periphery of said second cladding and having a fourth refractive index lower than the third refractive index.

18. A dispersion-compensating optical fiber according to claim 17, wherein said core region has a relative refractive index difference of 2.0% or more but 3.0% or less with reference to said third cladding.

19. A dispersion-compensating optical fiber according to claim 17, wherein said first cladding has a relative refractive index difference of -0.4% or less with reference to said third cladding.

20. A dispersion-compensating optical fiber according to claim 17, wherein the ratio (S_{DCF}/D_{DCF}) changes by 10% or less when an outer diameter of said second cladding changes by 2%.

5 21. An optical transmission line, comprising:
a dispersion-compensating optical fiber according to claim 1; and

a dispersion-shifted optical fiber connected to said dispersion-compensating optical fiber according to claim 1, said dispersion-shifted optical fiber having, at a
10 wavelength of 1550 nm, characteristics of:

a chromatic dispersion of +2 ps/nm/km or more but +10 ps/nm/km or less; and

a dispersion slope of +0.04 ps/nm²/km or more but +0.12
15 ps/nm²/km or less.

22. An optical transmission line according to claim 21, wherein a deviation of an average chromatic dispersion of said entire optical transmission line is 0.2 ps/nm/km or less in a wavelength band of 1535 nm or more but 1560
20 nm or less.

23. An optical transmission line according to claim 22, wherein the deviation of the average chromatic dispersion of said entire optical transmission line is 0.2 ps/nm/km or less in a wavelength band of 1535 nm or more but 1600
25 nm or less.

24. A dispersion-compensating module including a

dispersion-compensating optical fiber according to claim 1 in a state that said dispersion-compensating optical fiber is wound like a coil so as to form a module.

25. A dispersion-compensating module according to claim 24, wherein said dispersion-compensating module has a total loss is 7 dB or less in a wavelength band of 1535 nm or more but 1565 nm or less when a dispersion-compensating amount is -640 ps/nm at a wavelength of 1550 nm.

26. A dispersion-compensating module according to claim 25, wherein the total loss is 7 dB or less in a wavelength band of 1535 nm or more but 1610 nm or less.

27. A dispersion-compensating module according to claim 24, wherein said dispersion-compensating module has a total loss of 3 dB or less in a wavelength band of 1535 nm or more but 1565 nm or less when a dispersion-compensating amount is -320 ps/nm at a wavelength of 1550 nm.

28. A dispersion-compensating module according to claim 27, wherein the total loss is 3 dB or less in a wavelength band of 1535 nm or more but 1610 nm or less.

29. A dispersion-compensating optical fiber having a core region extending along a predetermined axis and a cladding region surrounding around the outer periphery of said core region, said dispersion-compensating optical fiber having, at a wavelength of 1550 nm, characteristics of:

a chromatic dispersion D_{DCF} of -40 ps/nm/km or less;
a ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the

chromatic dispersion D_{DCF} of 0.005/nm or more; and
an effective area of $16\mu\text{m}^2$ or more.

30. A dispersion-compensating optical fiber
according to claim 29, wherein the effective area is 20
5 μm^2 or more at the wavelength of 1550 nm.

31. A dispersion-compensating optical fiber having
a core region extending along a predetermined axis and a
cladding region surrounding around the outer periphery of
said core region, said dispersion-compensating optical fiber
10 having, at a wavelength of 1550 nm, characteristics of:

a chromatic dispersion D_{DCF} of -40 ps/nm/km or less;
a ratio (S_{DCF}/D_{DCF}) of dispersion slope S_{DCF} to the
chromatic dispersion D_{DCF} of 0.005/nm or more; and
a transmission loss of 0.5 dB/km or less.

15

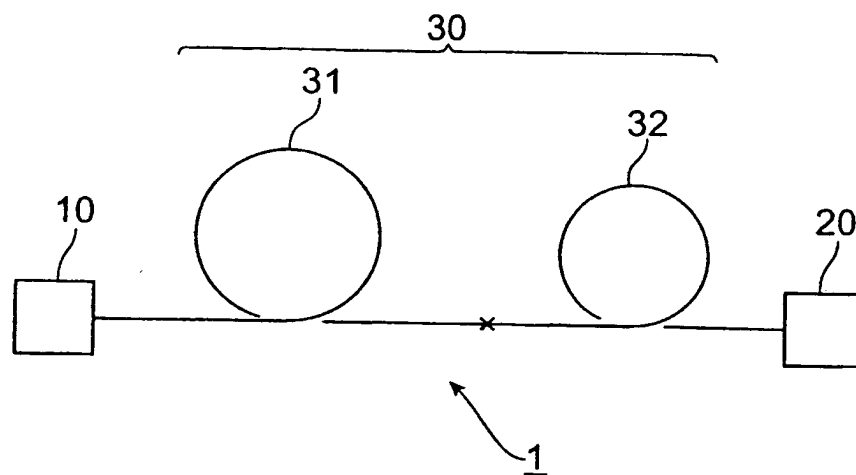
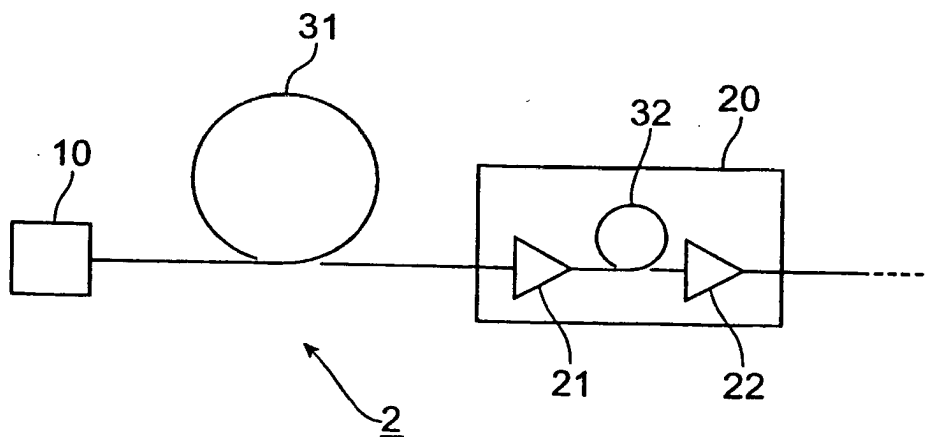
Fig.1**Fig.2**

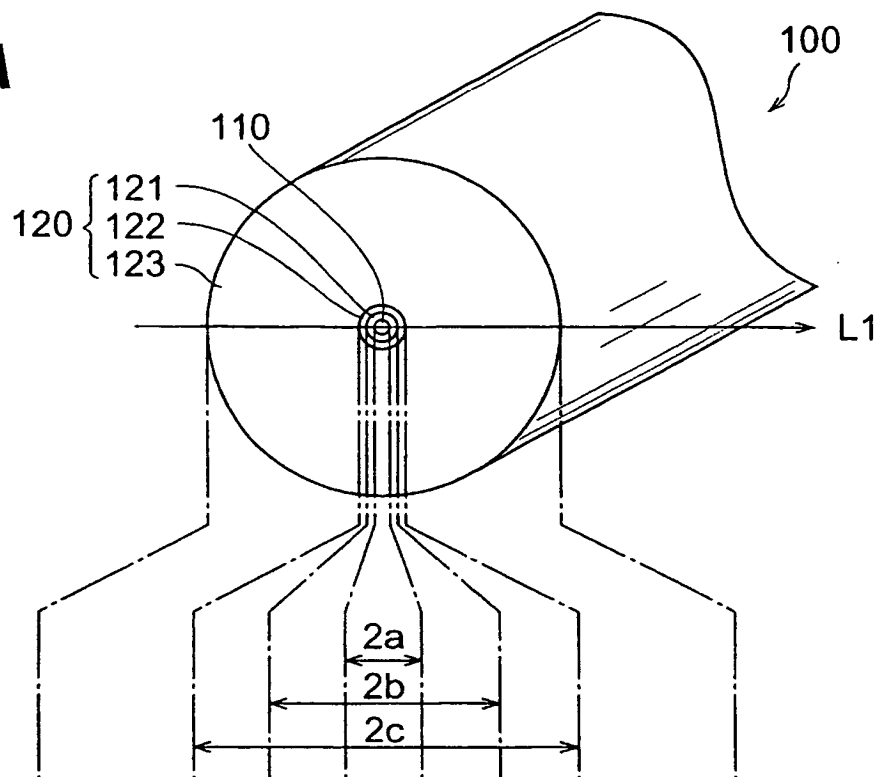
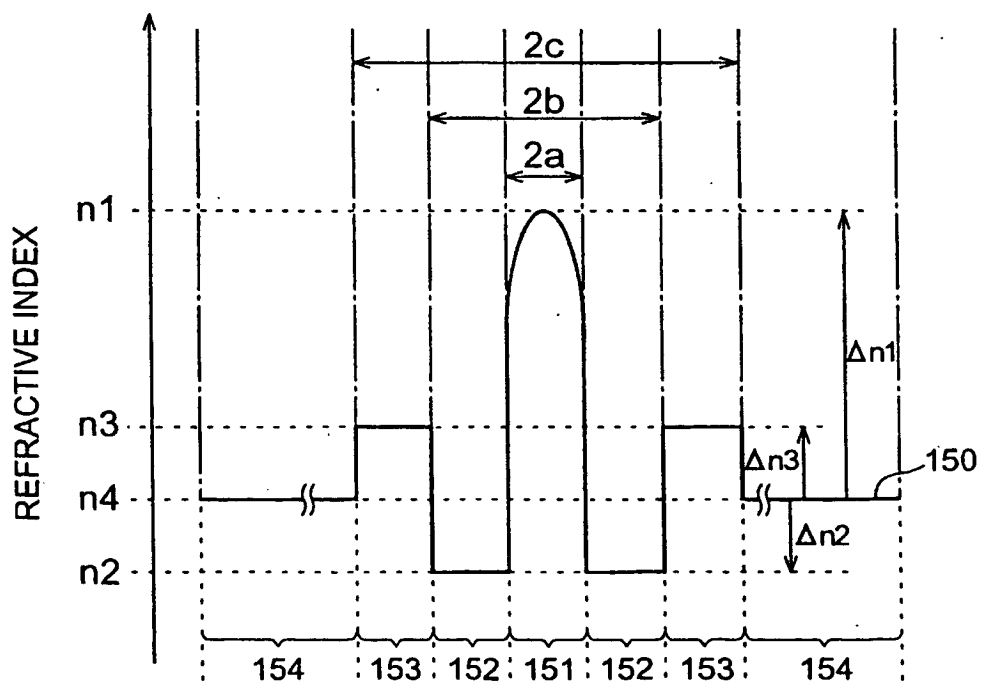
Fig.3A**Fig.3B**

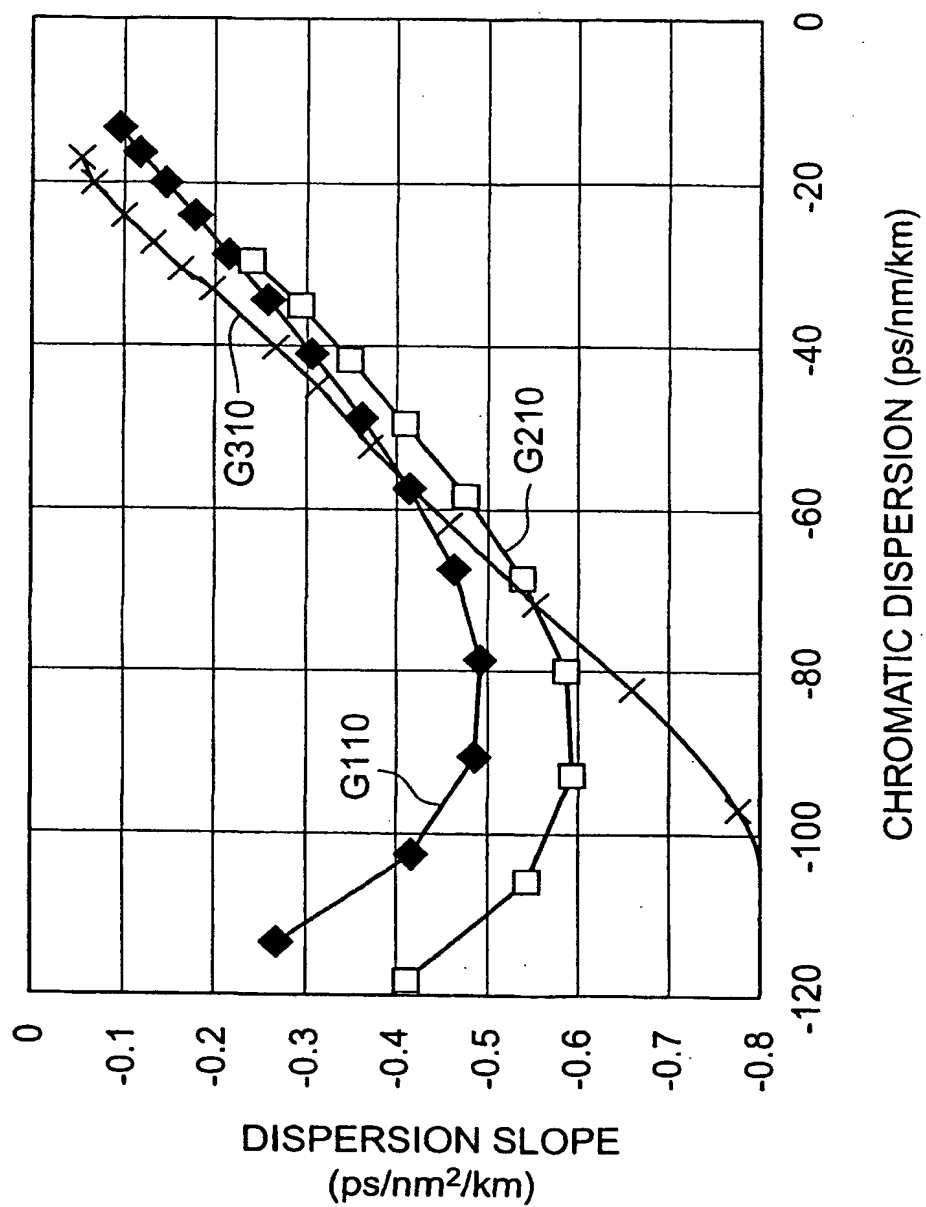
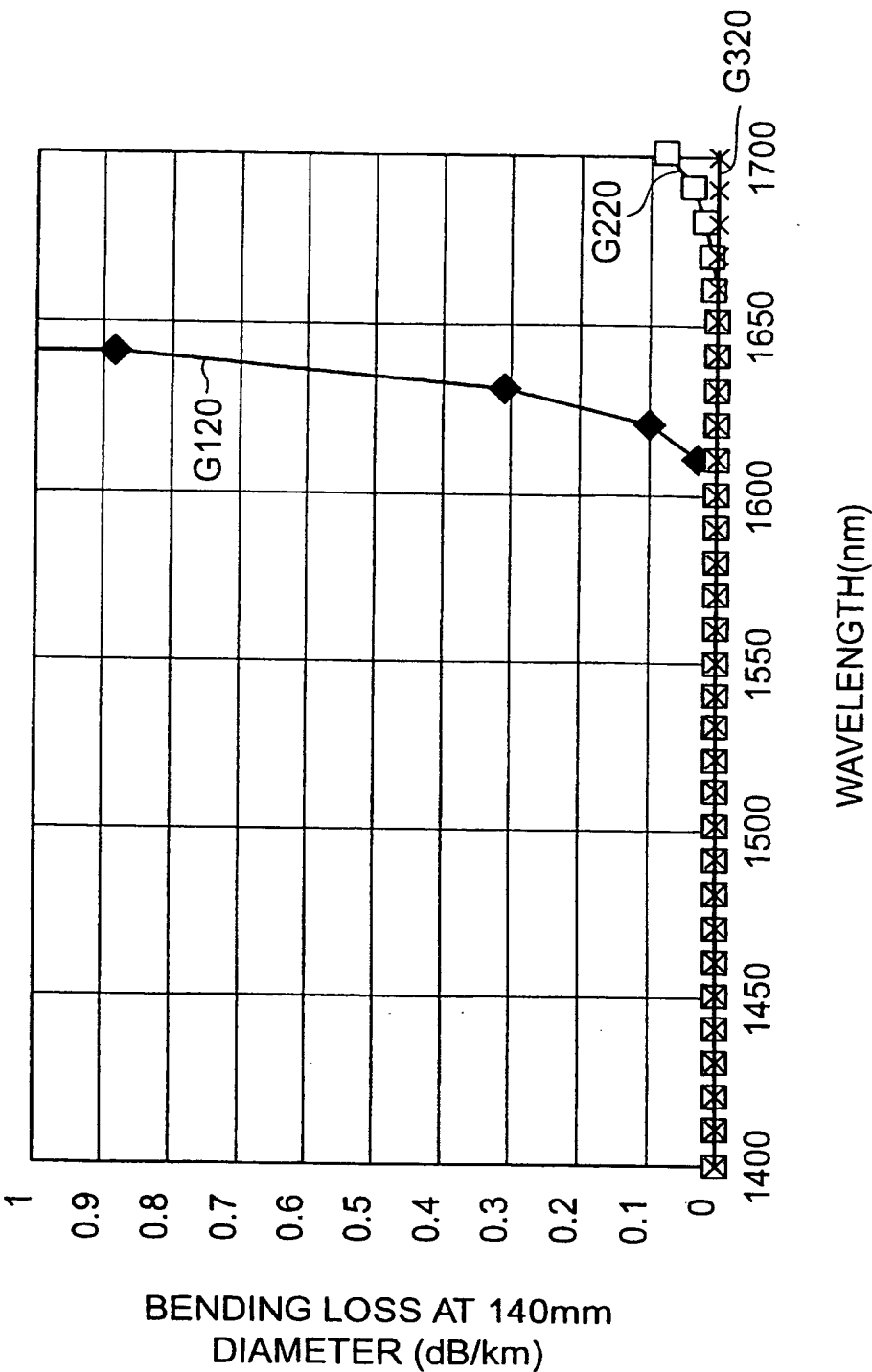
Fig.4

Fig.5



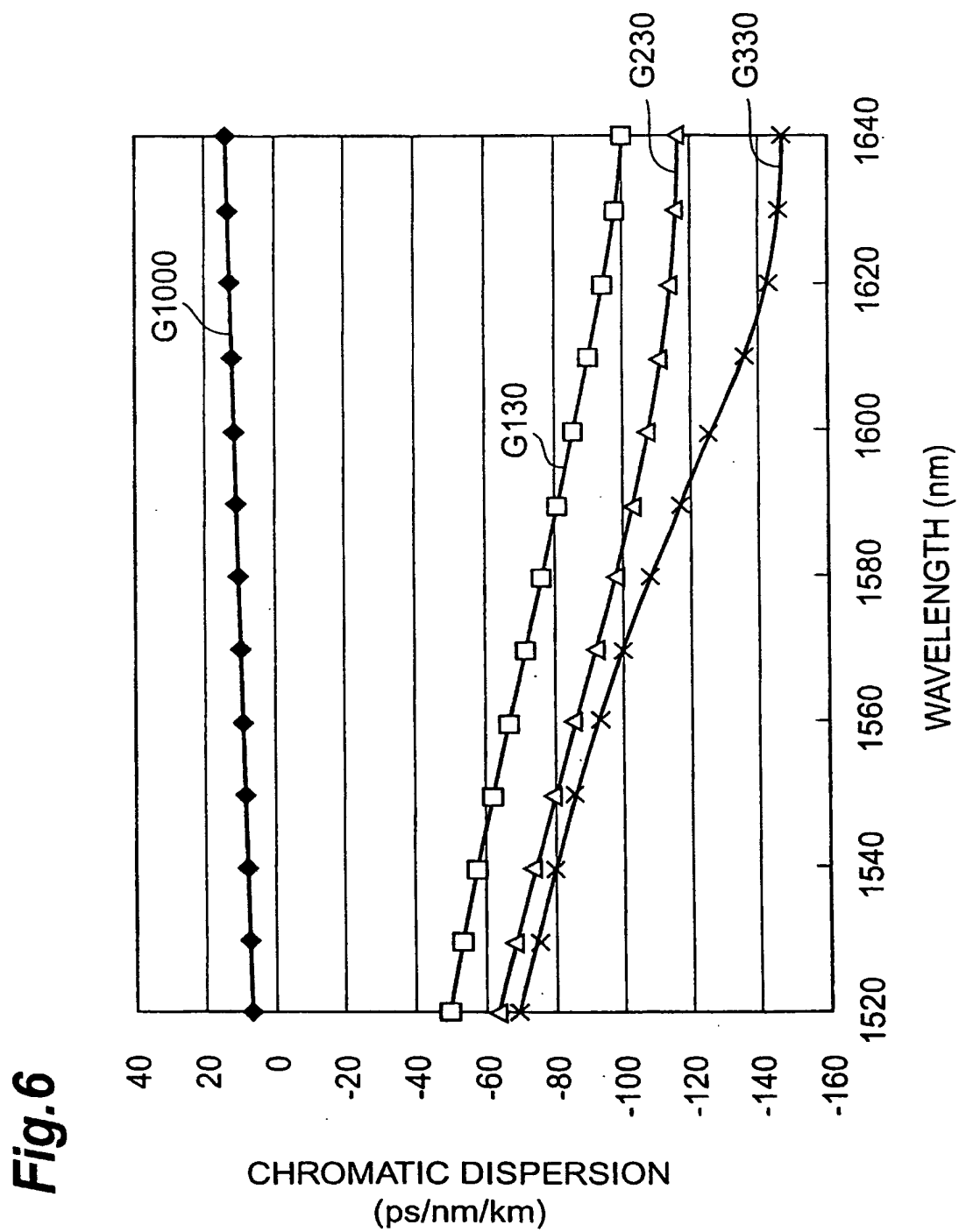


Fig. 7

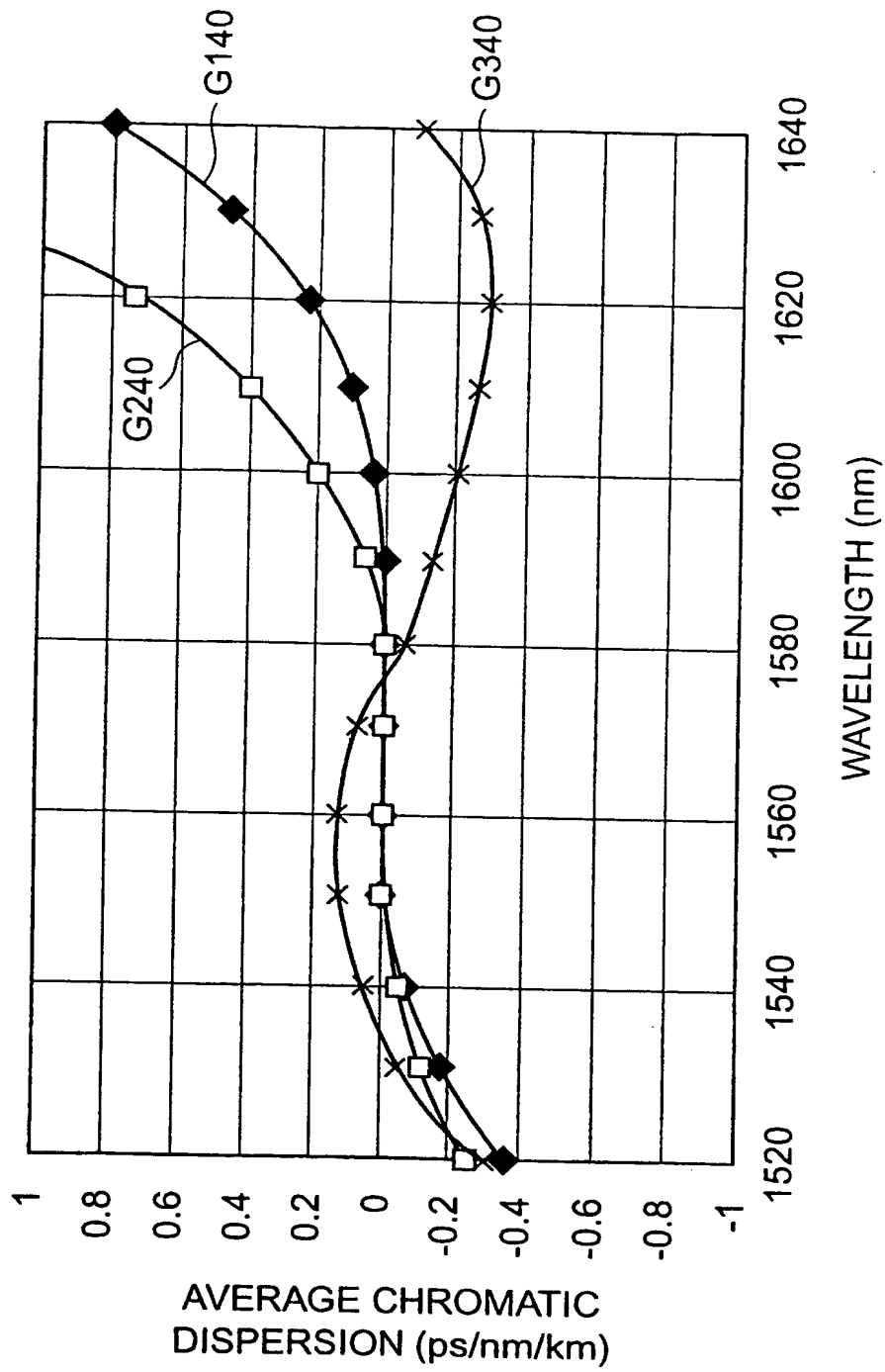
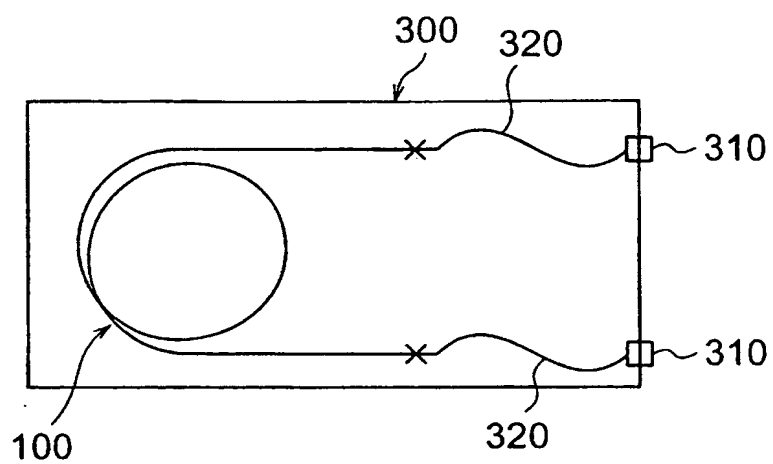


Fig.8

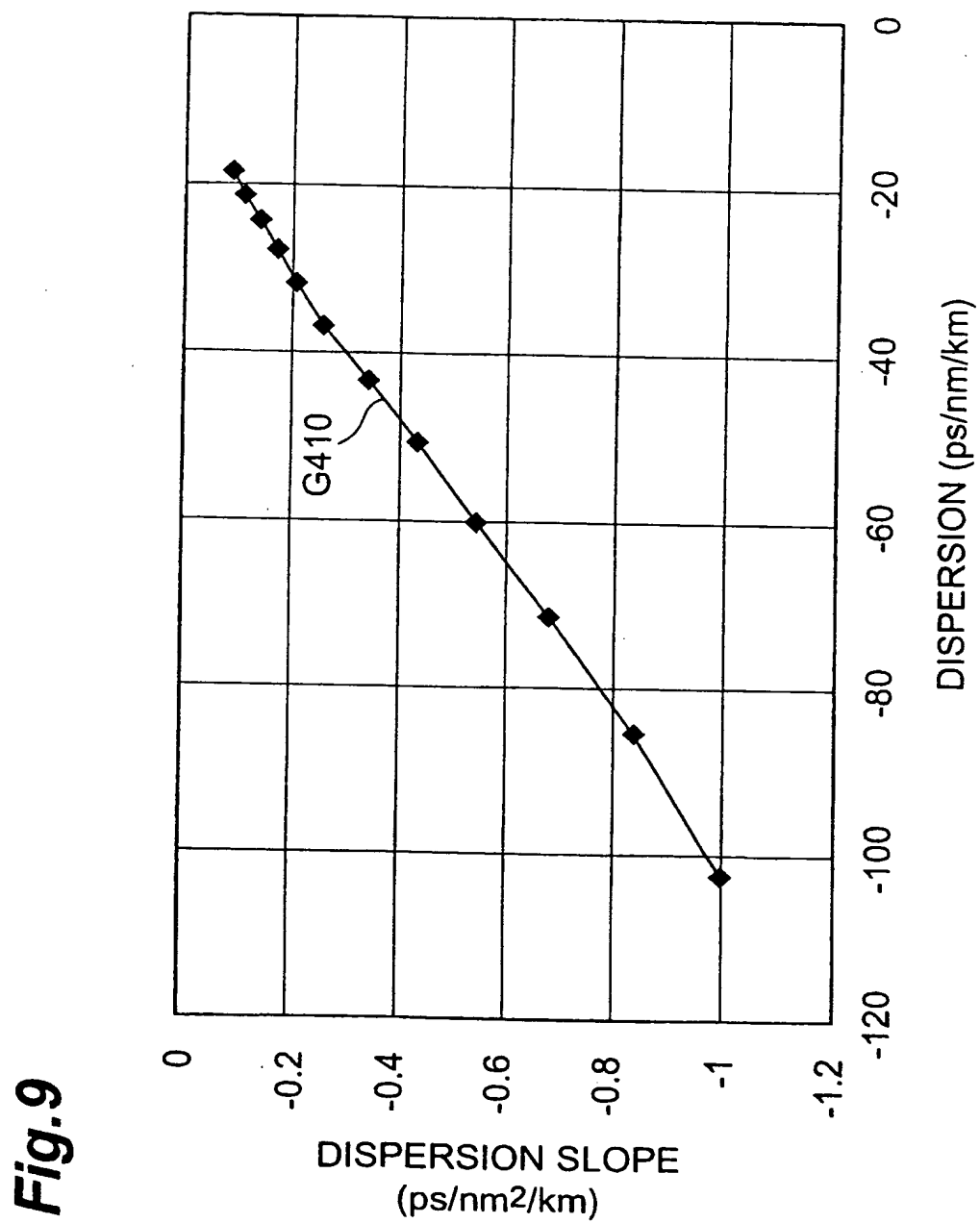
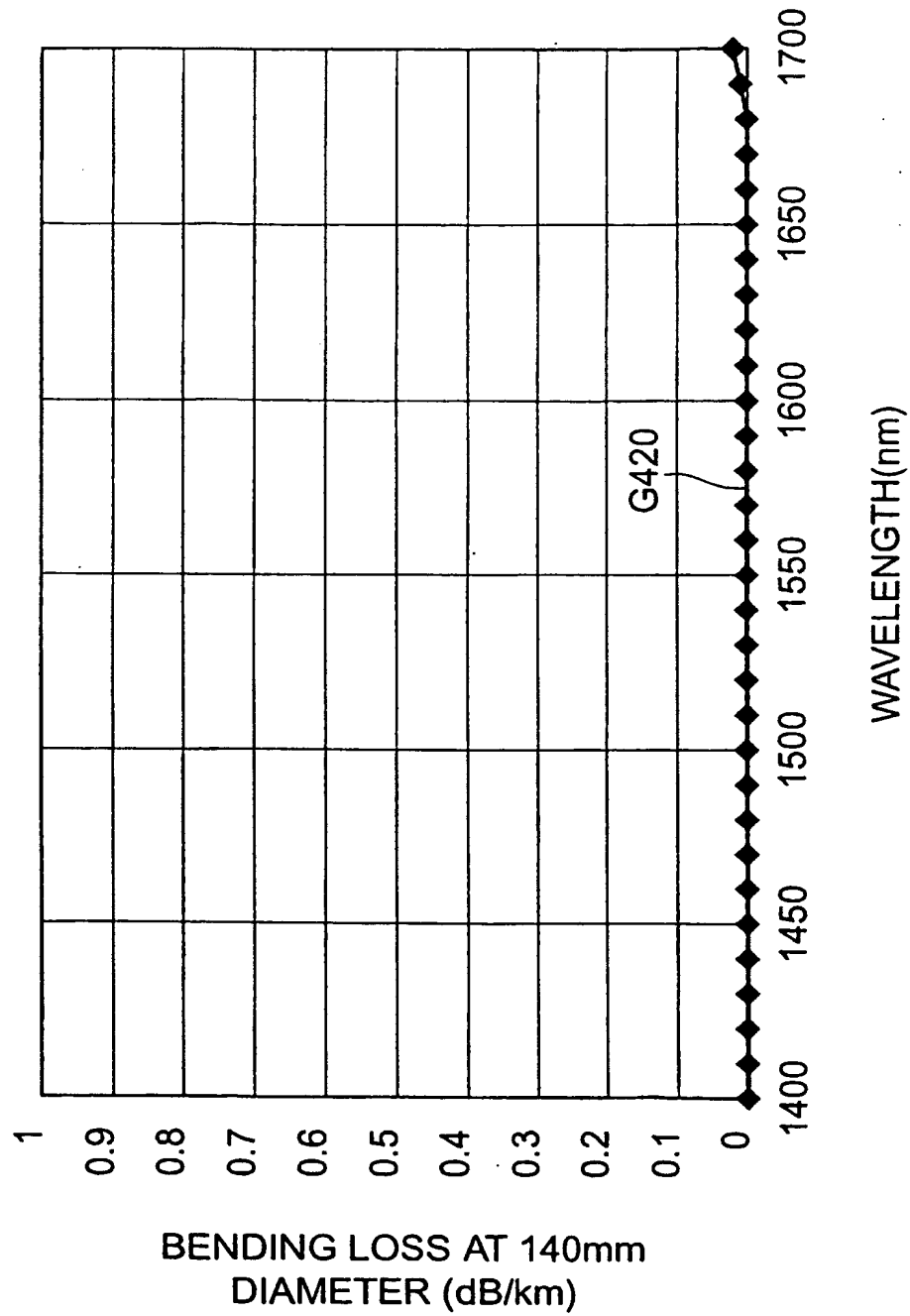


Fig.10



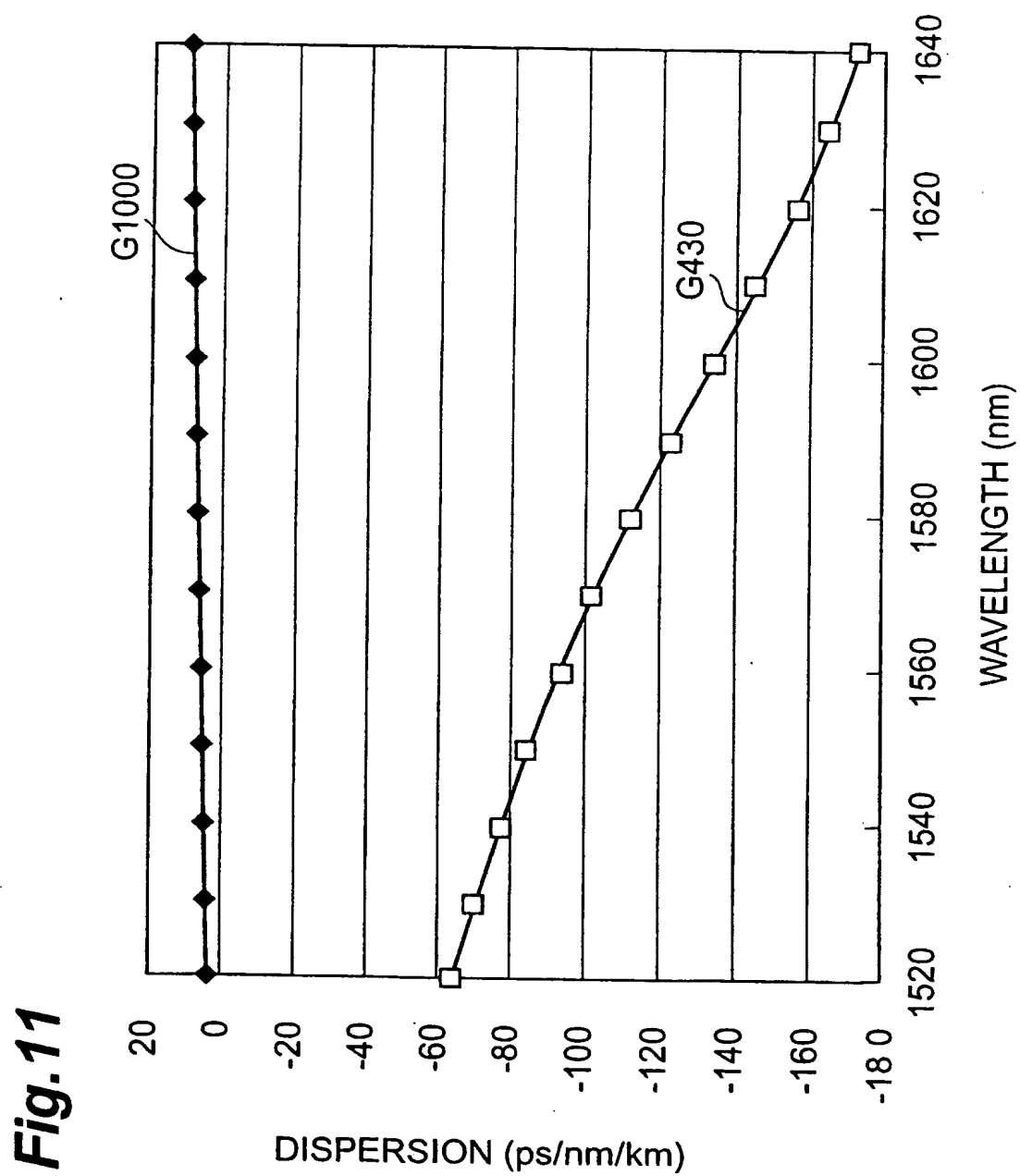
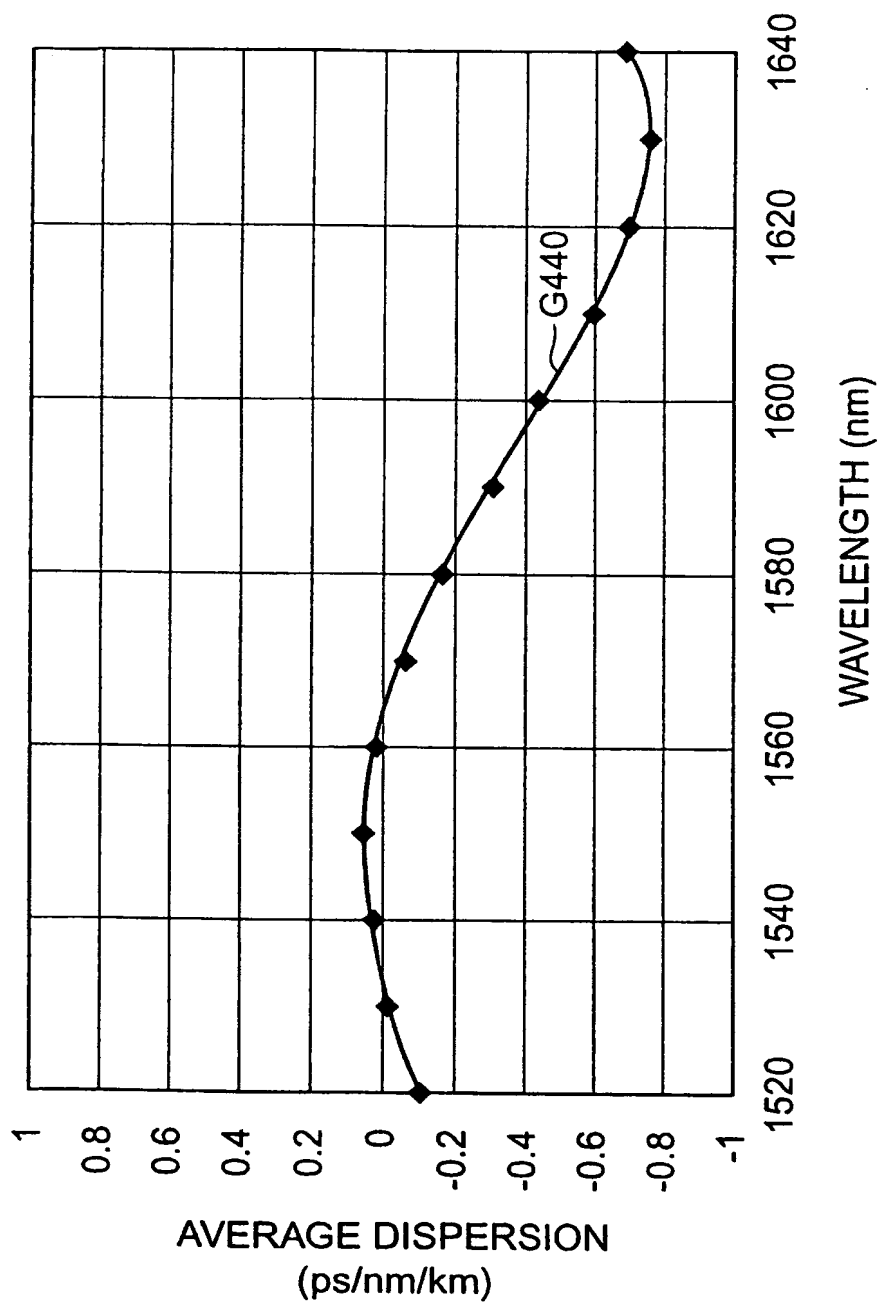


Fig.12

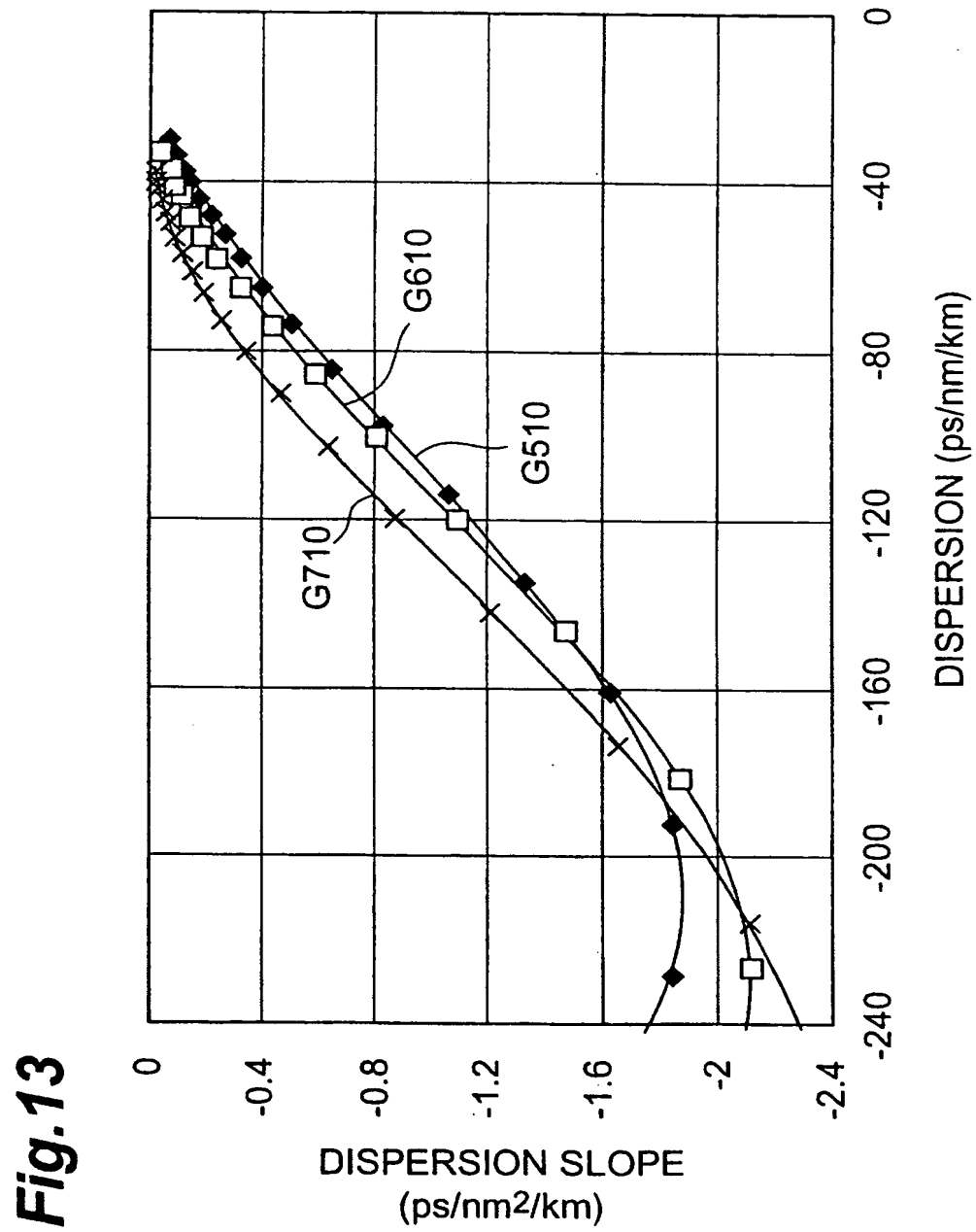


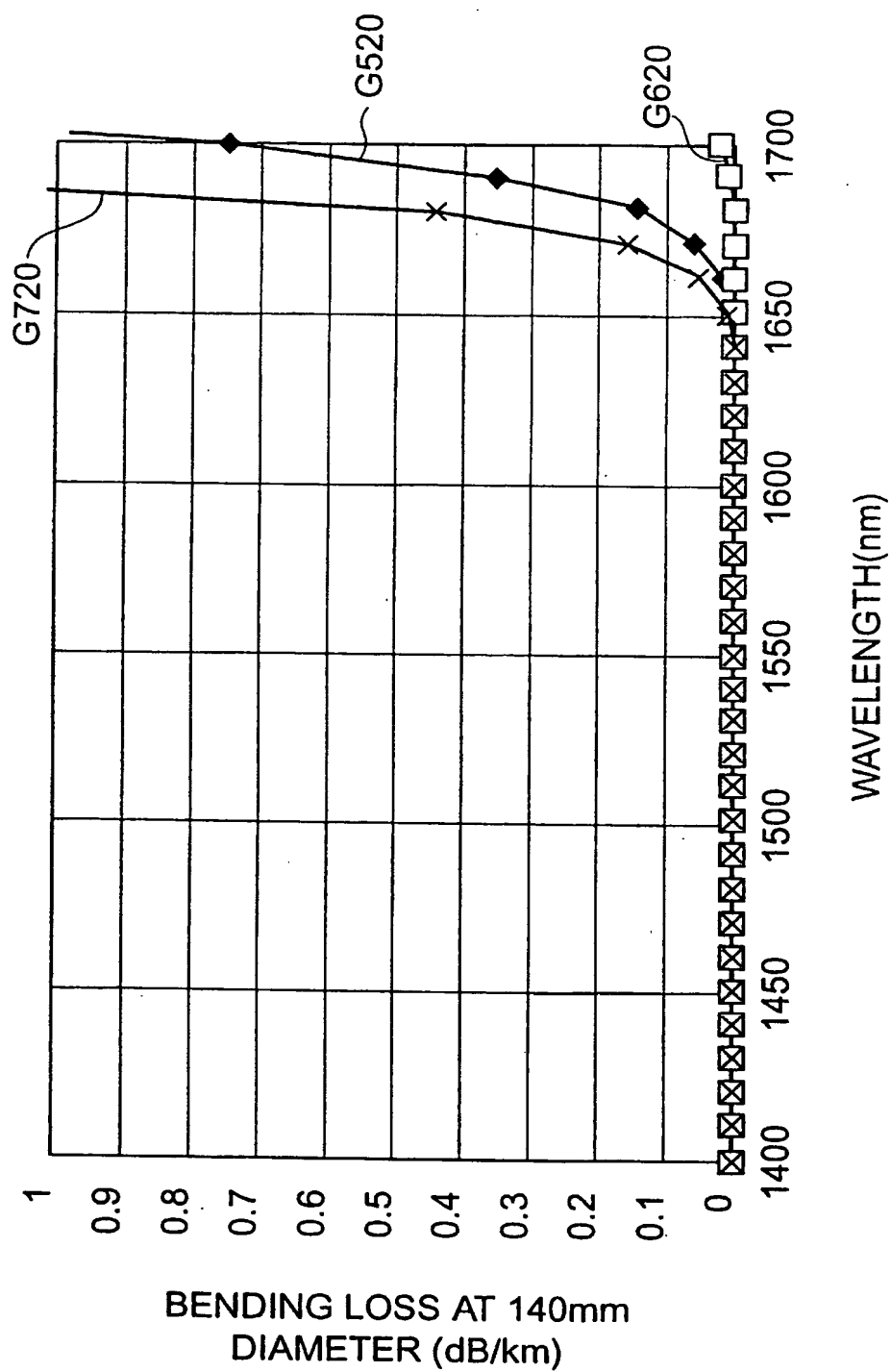
Fig.14

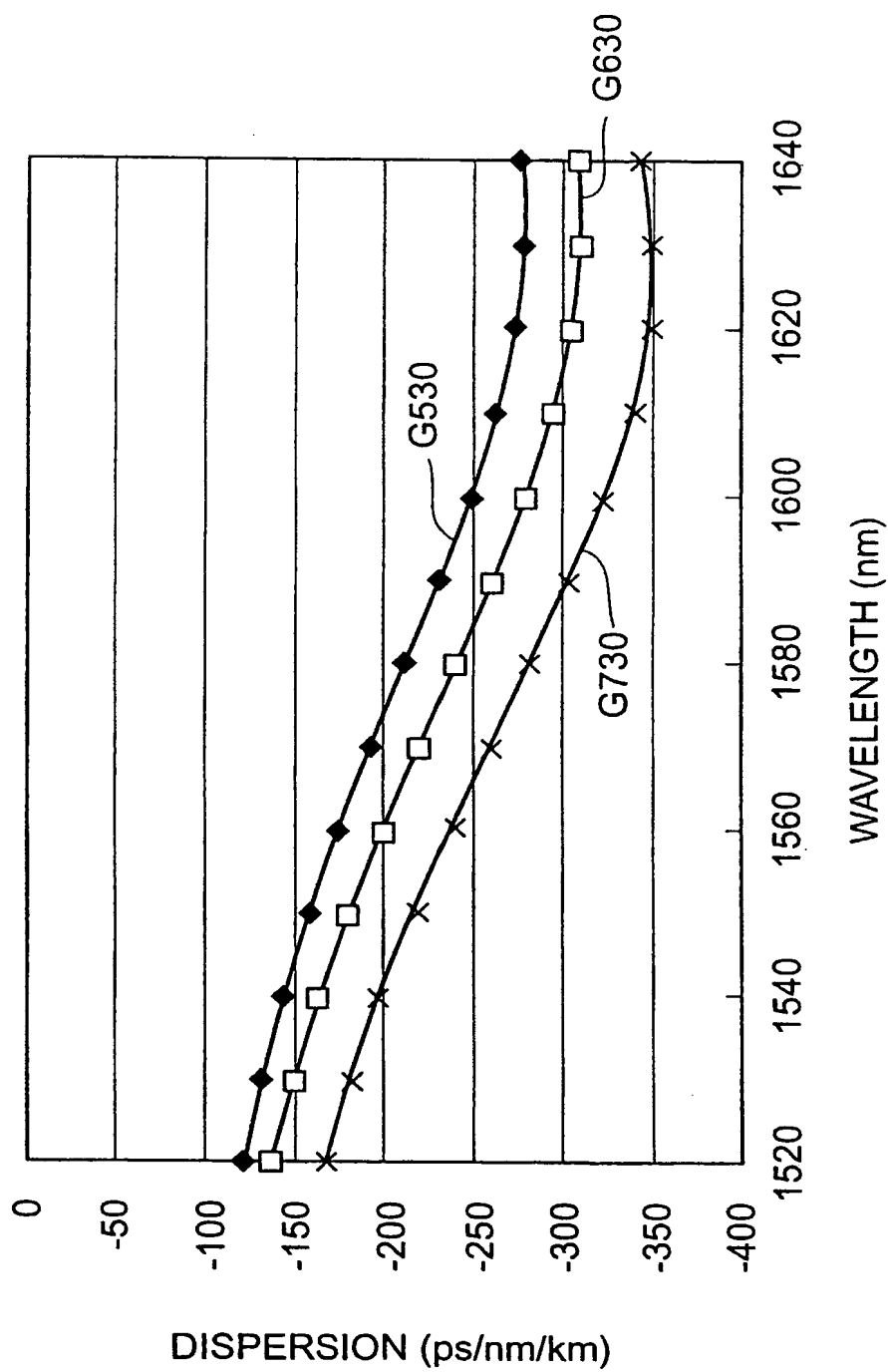
Fig.15

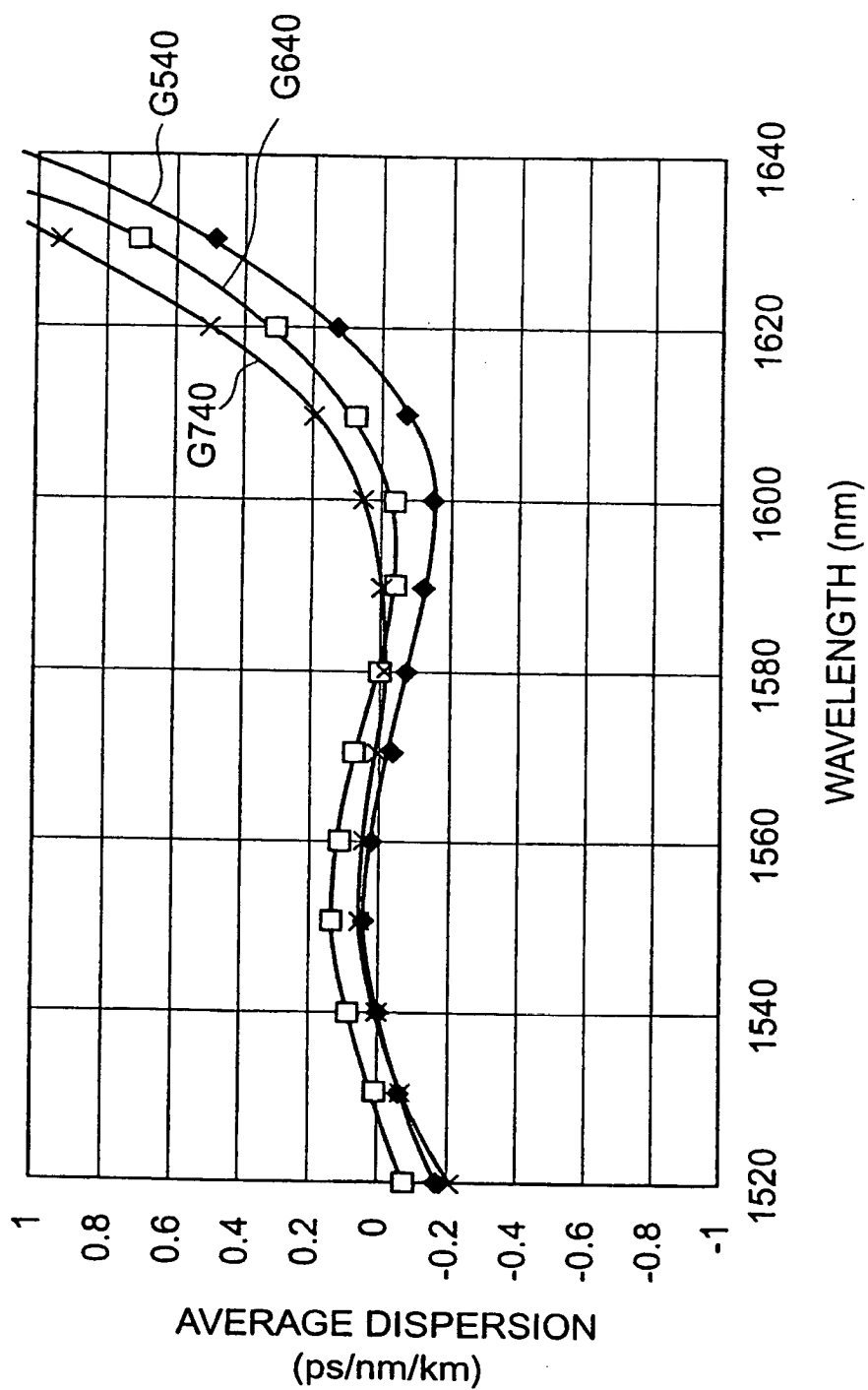
Fig.16

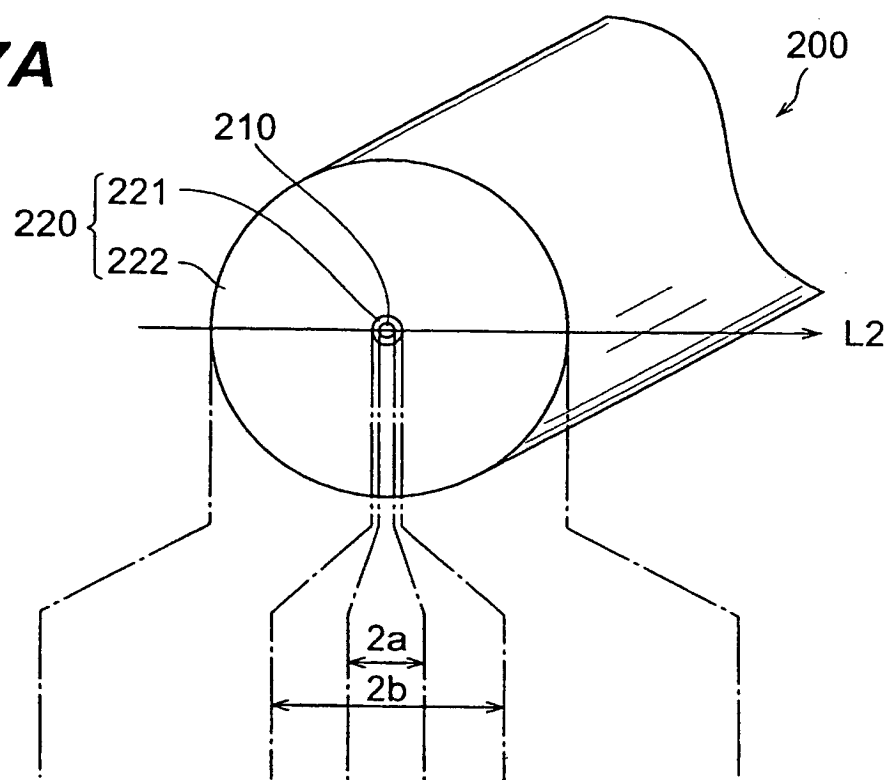
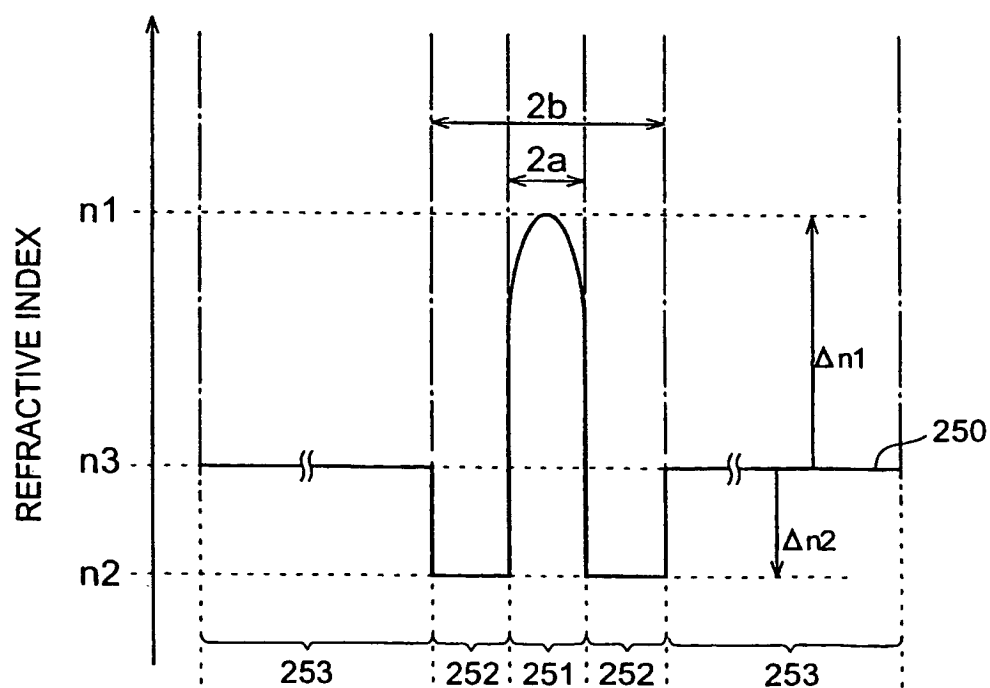
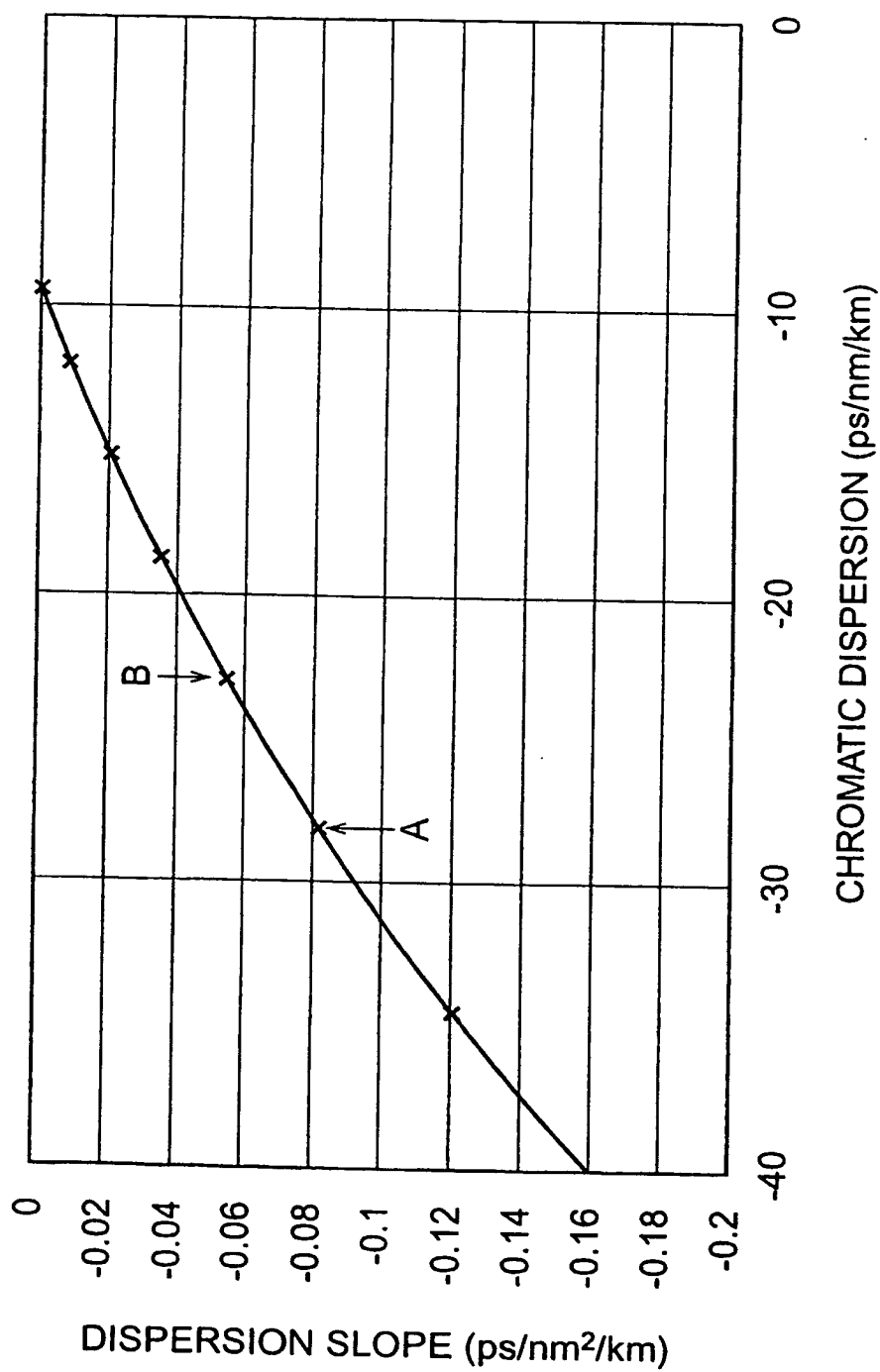
Fig.17A**Fig.17B**

Fig.18

INTERNATIONAL SEARCH REPORT

In International Application No.

PCT/JP 00/08528

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 G02B6/22

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

WPI Data, INSPEC, EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 448 674 A (VENGSARKAR ASHISH M ET AL) 5 September 1995 (1995-09-05)	1,8-11
Y	abstract; figures column 3, line 49 -column 4, line 68 column 5, line 7 - line 66 ---	17-19, 21,24
Y	US 5 995 694 A (AKASAKA YOUICHI ET AL) 30 November 1999 (1999-11-30) abstract; figure 2 column 2, line 14 - line 62 column 6, line 64 -column 7, line 5 --- -/--	21,24

☒ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

* Special categories of cited documents :

- *A* document defining the general state of the art which is not considered to be of particular relevance
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- *&* document member of the same patent family

Date of the actual completion of the international search

27 August 2001

Date of mailing of the international search report

31/08/2001

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Faderl, I

INTERNATIONAL SEARCH REPORT

In International Application No

PCT/JP 00/08528

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	ANTOS A J ET AL: "DESIGN AND CHARACTERIZATION OF DISPERSION COMPENSATING FIBER BASED ON THE LPO1 MODE" JOURNAL OF LIGHTWAVE TECHNOLOGY,US,IEEE. NEW YORK, vol. 12, no. 10, 1 October 1994 (1994-10-01), pages 1739-1744, XP000469527 ISSN: 0733-8724 page 1740, paragraph B -page 1741; figures 2-4	17-19
P,X	EP 1 000 909 A (HERAEUS QUARZGLAS) 17 May 2000 (2000-05-17) abstract; figures 3A,3B	1
E	WO 01 01178 A (MUKASA KAZUNORI ;FURUKAWA ELECTRIC CO LTD (JP)) 4 January 2001 (2001-01-04) abstract; figure 1	1
A	FR 2 761 483 A (FURUKAWA ELECTRIC CO LTD) 2 October 1998 (1998-10-02) abstract; figure 4C	1
A	EP 0 935 146 A (CORNING INC) 11 August 1999 (1999-08-11) figure 8; tables 1-FIG.8	1
A	US 5 838 867 A (KANAMORI HIROO ET AL) 17 November 1998 (1998-11-17) cited in the application page 1; figure 5A	1
A	DE 198 39 870 A (DEUTSCHE TELEKOM AG) 9 March 2000 (2000-03-09) abstract; figure 1	1

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

Continuation of Box I.2

Claims Nos.: 2-7,12-16,20,22,23,25-31

Present claims (2-7,12-16,20,22,23,25-31) relate to an optical fiber defined by reference to one of the following desirable characteristics or properties:

- chromatic dispersion values
- dispersion slopes
- different ratios of the dispersion slope divided by chromatic dispersion value
- effective areas at certain wavelengths
- cut-off wavelengths
- changement of the ratio of dispersion slope divided by chromatic dispersion
- transmission loss per kilometer, etc.

These properties are defined by the choice of the refractive index profile, applied materials and eventually the fabrication method and how this fiber is used.

The claims cover all products having this characteristic or property, whereas the application provides support within the meaning of Article 6 PCT and/or disclosure within the meaning of Article 5 PCT for only a very limited number of such products. In the present case, the claims so lack support, and the application so lacks disclosure, that a meaningful search over the whole of the claimed scope is impossible. Independent of the above reasoning, the claims also lack clarity (Article 6 PCT).

For example, the claims do not precise

- any refractive index for the second cladding
- any diameter: neither core, nor first, nor second cladding.

By omitting these technical features a meaningful search in the field of dispersion-compensated or dispersion-shifted fibers is not possible as this kind of profile - generally speaking a W-profile with one first suppressed cladding layer - is already known to the person skilled in the art.

In the claims, therefore an attempt is made to define the product by reference to a result to be achieved. Again, this lack of clarity in the present case is such as to render a meaningful search over the whole of the claimed scope impossible.

Consequently, the search has been carried out for those parts of the claims which appear to be clear, supported and disclosed, namely those parts relating to the optical fibers disclosed in the description in the embodiments 1-7 (pages 27-29: embodiments 1-3; page 36: embodiment 4; pages 41-42: embodiments 5-7) as well as the devices relating to this type of fiber. The claims 1,8-11,17-19,21,24 without the elements from the description would not be searcheable neither because they also lack clarity.

The applicant's attention is drawn to the fact that claims, or parts of claims, relating to inventions in respect of which no international

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

search report has been established need not be the subject of an international preliminary examination (Rule 66.1(e) PCT). The applicant is advised that the EPO policy when acting as an International Preliminary Examining Authority is normally not to carry out a preliminary examination on matter which has not been searched. This is the case irrespective of whether or not the claims are amended following receipt of the search report or during any Chapter II procedure.

INTERNATIONAL SEARCH REPORT

Information on patent family members

In International Application No

PCT/JP 00/08528

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